

Limits of Optical Fibre Communication Systems

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ABSTRACT

In this presentation, we will review the historical evolution of performance predictions for optical communication systems, including single channel systems, soliton systems and high spectral density coherent systems. We will describe how such predictions have been made from the outset of optical communications research and their present form, accurately predicting the performance of coherently detected communication systems and establishing the fundamental limits of nonlinearity compensation.

Keywords: nonlinear analysis, optical communications, coherent, four wave mixing.

1. INTRODUCTION

Theoretical studies of the performance of optical transmission systems have always sought to establish a practical limit. Since 2009, this limit has been commonly called the “nonlinear Shannon limit” [1-2] and a consensus has begun to form regarding the actual maximum achievable performance. When taking into account the upper limit of the throughput of optical transmission systems and the constant growth (40% per annum [3]) in traffic demand, an optical “capacity crunch” has now been predicted [4-5]. This will necessitate a shift in the business model for telecommunications service providers. The theoretical prediction of the performance of optical communication systems dates back to the 1960’s [6-7]. In this presentation, we will trace their evolution and review their contemporary relevance for both directly and coherently detected systems. We will examine the different models, and extend the analysis to systems which compensate for nonlinear impairments.

2. NONLINEARITY MODELS IN SINGLE MODE FIBRE

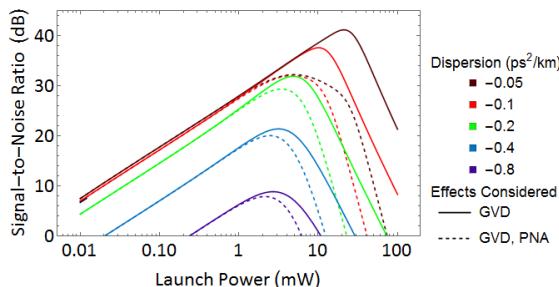


Figure 1. Predicted signal to noise ratio for a 40 Gbaud ASK-DD over ten 50km spans.

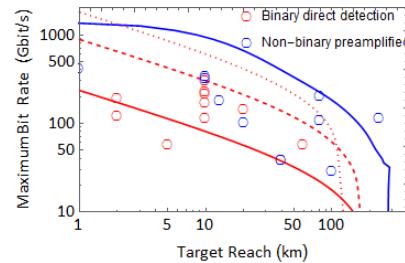


Figure 2. Maximum bit rate for single wavelength systems with direct detection as a function of transmission length over single mode fibre.

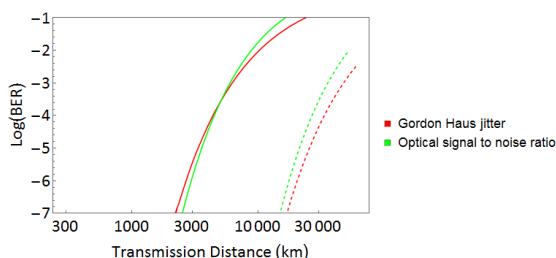


Figure 3. 33 Gbit/s on-off keyed soliton system, 34 km spacing and optimised pulse width. Solid: dispersion 16 fs/nm/km. Dashed: dispersion of -1 ps/nm/km for 32 km and 16 ps/nm/km for 2 km.

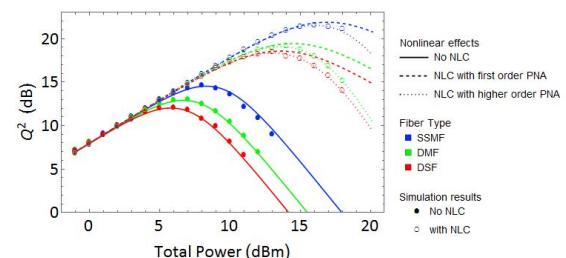


Figure 4. Simulated and predicted performance of lumped system with amplifier noise figure of 6dB and passing 8 channel, 28 Gbaud PM-QPSK Nyquist WDM system over 12 spans of 100 km [8]

Figures 1-4 (adapted from [8]) illustrate the performance predictions of various models including; the combined effects of self-phase modulation and dispersion for single wavelength systems (solid lines, Fig. 1) [9-11], parametric noise amplification (dashed lines, Fig. 1) [12-13], comparison of the predictions from these models with reported direct detection results (Fig. 2, see [8] for references to experimental results), soliton transmission systems with and without dispersion management (Fig. 3) [14-17], and the contemporary integration of four-wave mixing efficiencies under the assumption of Gaussian noise like input signals (Fig. 4) [18-21] with and without nonlinearity compensation (ideal DBP [22]). All of the models presented appear to have remained accurate, provided that the approximations used to derive them are adhered to. For example,

Fig. 2 compares the predictions from 20th century models alongside 21st century experimental results aimed at data centre applications with no indication that the model is inaccurate.

Careful inspection of these models [8] reveals a consistent theme. For simple systems operating with high dispersion and making no attempt to compensate for the nonlinear effects, it is sufficient to calculate the combined effects of dispersion and nonlinear interactions among the signals. However, for low dispersion systems (Fig. 1-3) or systems with nonlinearity compensation (Fig. 3-4), the nonlinear interaction between the signal and noise must be taken into account in order to attain accurate performance limits. For a system employing in-line optical amplification, differences in growth rates between the various nonlinear interactions impact their relative strength. This is illustrated in Fig. 5 which shows that for single mode fibre systems that deploy 20 to 40 amplifiers and for shorter systems with nonlinearity compensation, parametrically amplified noise [12-13, 21-24] is dominant, but for transoceanic systems, the process of nonlinear phase noise [25] is of increasing significance.

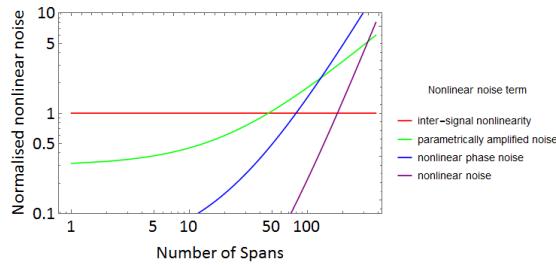


Figure 5. Relative impact of nonlinear interactions involving amplified spontaneous emission, with respect to inter-signal nonlinearity for a 20dB optical signal to noise ratio after one amplifier.

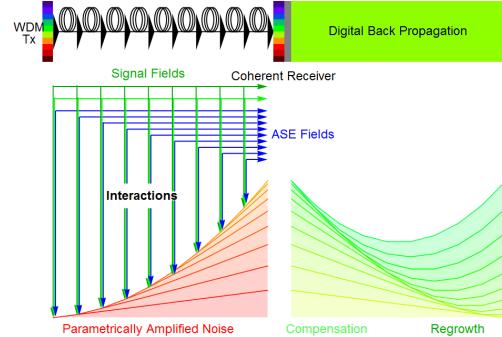


Figure 6. Evolution of parametrically amplified noise in a 9 span system with DBP.

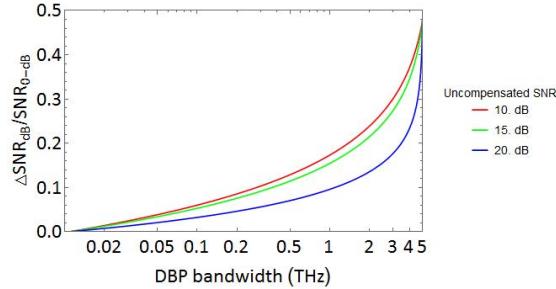


Figure 7. Predicted performance gain (50 spans) for 5 THz systems normalised to the original signal to noise ratio as a function of DSP bandwidth.

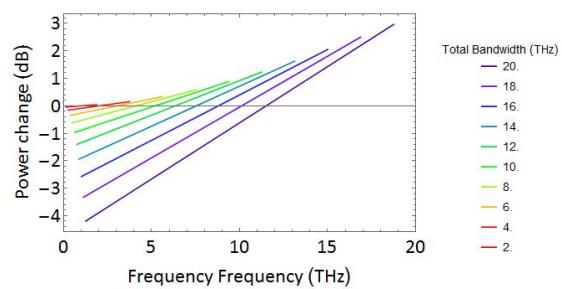


Figure 8. Approximate impact of inter-signal Raman power transfer over a 100 km Raman amplified span as a function of channel position.

As shown in Fig. 5, the majority of the nonlinear noise in many optical transmission systems is deterministic interaction between signals (assuming point-to-point transmission and cooperation between receivers). Compensating for inter-signal nonlinearity could, in principle, reduce the nonlinear noise by an order of magnitude and so enable higher launch powers and improved system performance [22, 26-27]. For a multi-channel system, it is unlikely that a single receiver would process the system and the practical limit in the ability to improve the signal to noise ratio appears to be around 1 – 2 dB [28]. However, by resorting to optical combs, significant gains are possible for isolated super-channels propagating without neighbours [29-31], and in this case the system becomes limited by parametric noise amplification. The evolution in this type of nonlinear noise for a system employing digital back-propagation is shown in Fig. 6, which shows clearly that it is not possible to fully eliminate parametric noise amplification. Parametric noise amplification thus sets a (higher) limit on the performance of an optical communication system, where the maximum signal to noise ratio in dB after ideal nonlinearity compensation is 1.5 times the maximum signal to noise ratio without compensation (less 0.5 dB to account for higher order nonlinearity) [32]. However, the Shannon limit indicates that increasing the used bandwidth is exponentially more favourable than increasing the signal-to-noise ratio and so systems designers will occupy all available bandwidth before compensating nonlinearity. In the context of a fully populated system, the reach doubling and tripling achieved with isolated super channels is unlikely to be achieved in a fully loaded transmission system unless the superchannel occupies the entire system bandwidth, as shown in Fig. 7.

3. SCATTERING EFFECTS

The theoretical models that describe the performance of optical transmission system often concentrate on the modelling of the Kerr nonlinear effects. However, the inelastic nonlinear effects of the optical fiber, such as

Brillouin and Raman scattering [33], may also degrade the performance of the transmission system. Brillouin scattering limits the signal power spectral density (typically around 0.5 W/GHz compared to less than 1 mW/GHz in Fig. 4), whilst Raman scattering predominantly results in gain tilts especially in broadband optical transmission systems (Fig. 8), but may also induce nonlinear noise.

4. NONLINEARITY MODELS IN FEW-MODE FIBRE

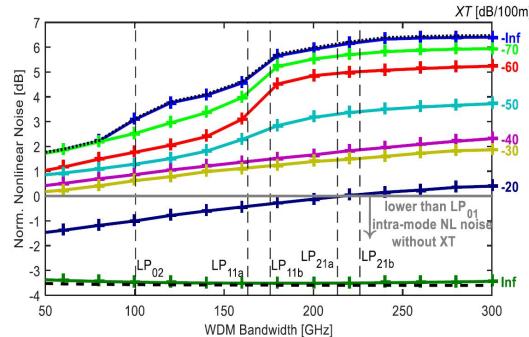


Figure 9. Total nonlinear noise power in LP01 as a function of WDM bandwidth showing Manakov predictions for strong (dashed) and weak (dotted) crosstalk and with fully stochastic simulations (solid).

nonlinear distortion below that of the isolated mode without mode coupling can be achieved.

5. PERFORMANCE METRICS

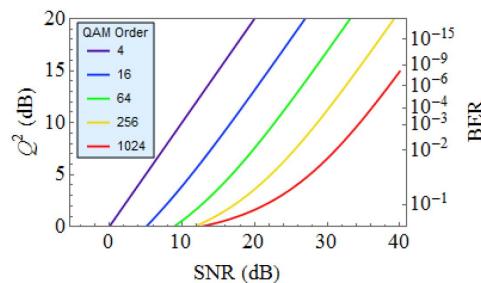


Figure 10. Relationship between performance metrics used in optical fibre communications.

non-binary formats the use of Q^2 prevails today. Assuming a definition of Q as “that Q factor for a QPSK signal which would give the same BER as the measured system”, Fig. 10 shows the relationship between Q^2 , signal to noise ratio and BER.

6. CONCLUSIONS

We have discussed the historical evolution of performance limit predictions. Whilst substantial gains are possible in practice, it has always been the case that the fundamental limit arises from the nonlinear interaction between the signal and noise fields, either in terms of parametric noise amplification, Gordon-Haus jitter, or nonlinear phase noise. Practical limits strongly depend on the degree to which the nonlinearity is compensated. For the foreseeable future (until fully populated WDM systems enjoy widespread deployment), it is unlikely that systems will be installed operating anywhere close to the new performance limits, although performance gains of up to 3-4dB should be possible.

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