

# Relative intensity noise transfer in high-order distributed amplification through ultra-long fiber cavities

Mercedes Alcón-Camas,<sup>1</sup> Juan Diego Ania-Castañón<sup>2,\*</sup>

<sup>1</sup>Photonics Research Group, School of Engineering and Applied Science, Aston University,  
Aston Triangle, Birmingham, B4 7ET, UK

<sup>2</sup>Instituto de Óptica “Daza de Valdés”, CSIC, C/ Serrano 121, 28006 Madrid, Spain

[\\*juan.diego@io.cfmac.csic.es](mailto:juan.diego@io.cfmac.csic.es)

## ABSTRACT

Among the different possible amplification solutions offered by Raman scattering in optical fibers, ultra-long Raman lasers are particularly promising as they can provide quasi-lossless second order amplification with reduced complexity, displaying excellent potential in the design of low-noise long-distance communication systems. Still, some of their advantages can be partially offset by the transfer of relative intensity noise from the pump sources and cavity-generated Stokes to the transmitted signal. In this paper we study the effect of ultra-long cavity design (length, pumping, grating reflectivity) on the transfer of RIN to the signal, demonstrating how the impact of noise can be greatly reduced by carefully choosing appropriate cavity parameters depending on the intended application of the system.

Ultra-long Raman fiber lasers, Raman amplification, RIN transfer, optical communications

## 1. Introduction

The advantages of distributed optical fiber Raman amplifiers [1,2] over traditional lumped optical amplification are well known, and include an improved noise performance and extended bandwidth. Standard conventional optical fibers are susceptible to Raman scattering, which can be used to provide Raman amplification without restriction to a particular range of wavelengths. This brings the opportunity of upgrading existing transmission systems through the implementation of Raman amplification, on its own or combined with other existing amplification solutions, increasing system performance and capacity. Recently, ultra-long Raman fiber lasers (URFLs) [3-7], in which transmission fiber acts as an ultra-long laser cavity that is used for signal amplification, have been shown to be able to further reduce signal power excursion, improving noise performance and presenting itself as an interesting alternative to high-order Raman amplification schemes.

Among the challenges of distributed Raman amplification, an important one is relative intensity noise (RIN) [8] transfer. This is a pump-to-signal noise transfer with origin in the intensity fluctuations of the pump laser source. Any fluctuation on the pump power will be reflected in a variation of signal gain, and thus be imprinted in the signal, creating an additional source of noise that, in some situations and with a low-quality pump source, can be as damaging a noise source as amplified spontaneous emission (ASE) itself.

The main contribution of this paper is the development of a numerical model for higher order distributed Raman amplifiers, in particular but not in exclusivity for ultra-long Raman fiber lasers. This numerical model allows us to investigate the effect of features design, such as span length, pump distribution and fiber Bragg gratings (FBGs) reflectivity, on the relative intensity noise transfer performance of the system.

## 2. Theoretical model

In order to describe our numerical model, we propose to study two particular Raman amplifier systems. They are schematically described in Figure 1. The first system corresponds to a bi-directionally pumped URFL, with pumps at 1366nm. It involves a conventional standard optical fiber confined between a pair of high reflectivity FBGs with a central wavelength of 1455nm, corresponding to the first Raman Stokes of the pump source. The optical fiber length considered for this work ranges from 1 to 100km. The pump power at 1366nm is coupled into the system through WDMs. The wavelength of the transmitted signal is at 1550nm, corresponding to the second Stokes of the pump source.

As the pump power injected at 1366nm grows above the lasing threshold for the fiber cavity, a first Stokes component around 1455nm is generated and trapped between the grating reflectors. This component will behave as a second pump source, providing a wide Raman gain bandwidth to the transmitted signal, located around the second Stokes wavelength of 1550 nm. This second-order cascading pumping structure provides reduced power excursion, and therefore, the system can provide quasi-lossless transparency around 1550nm for a particular range of pump powers.

The second distributed Raman amplifier system involves a conventional standard optical fiber, ranging from 1 to 100km similarly to the first system, but no reflectors at all. The optical fiber is bi-directionally pumped at the wavelengths 1366nm and 1455nm. The pump powers from both pump sources are coupled into the system through WDMs. The transmitted signal is, as before, at 1550nm, corresponding to the second Stokes of the pump source at 1366nm and the first Stokes of the pump source at 1455nm.

The way to operate this amplifier system will be as follows. We increase the pump power at 1366nm to the same level as it would be done within the same conditions of span length, pump distribution and type of fiber for the first system. Therefore, the power profile at 1366nm along the span length will be the same as the first system. Then, we calculate the initial power at 1455nm at each end of the fiber span for our first system and use exactly the same 1455nm power value for the pumps of our second system. This allows us to generate an equivalent amplifier system to the first one with exactly the same power distribution for 1366nm, 1455nm and the transmission wavelength 1550nm, but using an extra bi-directional pump source at 1455nm instead of using FBGs with the same center of wavelength. Hence, average power distributions inside the two amplifiers are identical, which will make it possible to perform a direct comparison of their respective RIN transfer performances.

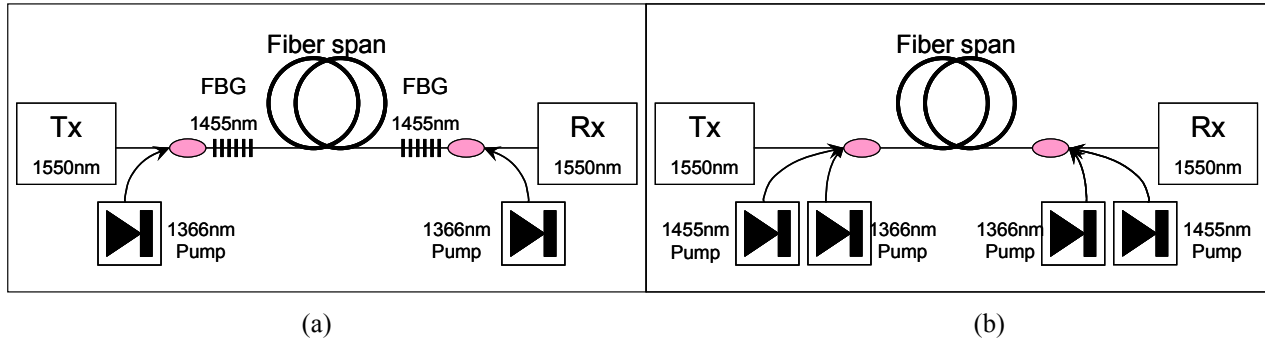


Figure 1: Schematic description of the studied bi-directional pumped Raman amplifier systems. (a) Ultra-long Raman fiber laser. (b) Equivalent power distribution system with dual pumping scheme.

As the power distribution should be the same for both systems given the same span length, pump power distribution and type of fiber, any difference on the RIN transfer values between these two systems is expected to come from the impact of having a laser cavity in the system instead of a dual wavelength pumping scheme.

Therefore we can quantify how the pump-noise transfer, with origin in the intensity fluctuation of the laser source due to spontaneous emission, evolves and it is magnified when using a laser cavity as amplifier.

The ordinary differential equations that describe mathematically our model are subdivided in two groups. On one side we have the set of equations 1 to 5 describing the average power evolution of pumps, signal and ASE noise along the length of the fiber for a second order Raman amplifier. These set of equations take in account all relevant effects, including pump depletion, ASE and double Rayleigh scattering (DRS) noise. A more extensive description of the average power performance for our first system can be found in reference [4].

$$\frac{dP_{P1}^{\pm}}{dz} = \mp \alpha_1 P_{P1}^{\pm} \mp g_1 \frac{\nu_1}{\nu_2} P_{P1}^{\pm} \left( P_{P2}^{+} + P_{P2}^{-} + 4h\nu_2 \Delta \nu_2 \left( 1 + \frac{1}{e^{h(\nu_1 - \nu_2)/K_B T} - 1} \right) \right) \pm \epsilon_1 P_{P1}^{\mp} \quad (1)$$

$$\begin{aligned} \frac{dP_{P2}^{\pm}}{dz} = & \mp \alpha_2 P_{P2}^{\pm} \pm g_1 \left( P_{P2}^{\pm} + 2h\nu_2 \Delta \nu_2 \left( 1 + \frac{1}{e^{h(\nu_1 - \nu_2)/K_B T} - 1} \right) \right) (P_{P1}^{+} + P_{P1}^{-}) \\ & \mp g_2 \frac{\nu_2}{\nu_s} P_{P2}^{\pm} \left( P_s^{+} + N_s^{+} + N_s^{-} + 4h\nu_s \Delta \nu_s \left( 1 + \frac{1}{e^{h(\nu_2 - \nu_s)/K_B T} - 1} \right) \right) \pm \epsilon_2 P_{P2}^{\mp} \end{aligned} \quad (2)$$

$$\frac{dP_s}{dz} = -\alpha_s P_s + g_2 P_s (P_{P2}^{+} + P_{P2}^{-}) \quad (3)$$

$$\frac{dN_s^{+}}{dz} = -\alpha_s N_s^{+} + g_2 \left( N_s^{+} + 2h\nu_2 \Delta \nu_2 \left( 1 + \frac{1}{e^{h(\nu_2 - \nu_s)/K_B T} - 1} \right) \right) (P_{P2}^{+} + P_{P2}^{-}) + \epsilon_s N_s^{-} \quad (4)$$

$$\frac{dN_s^{-}}{dz} = \alpha_s N_s^{-} - g_2 \left( N_s^{-} + 2h\nu_2 \Delta \nu_s \left( 1 + \frac{1}{e^{h(\nu_2 - \nu_s)/K_B T} - 1} \right) \right) (P_{P2}^{+} + P_{P2}^{-}) - \epsilon_s (P_s + N_s^{+}) \quad (5)$$

On the other hand, a different set of ODEs, equations 6 to 8, describe mathematically the evolution of the spectral densities of the amplitude noise along the span for a second order Raman amplification system. The cavity design parameters are introduced in the boundary conditions.

The subscripts 1, 2, and S denote the primary pump at 1366nm, secondary pump at 1455nm and signal at 1550nm respectively.

$$\frac{dn_1^{\pm}}{dz} + id_1^{\pm} \omega n_1^{\pm} = \mp \alpha_1 n_1^{\pm} \mp g_1 \frac{\nu_1}{\nu_2} P_1^{\pm} (n_2^{+} + n_2^{-}) \mp g_1 \frac{\nu_1}{\nu_2} (P_2^{+} + P_2^{-}) n_1^{\pm} \pm \epsilon_1 n_1^{\mp} \quad (6)$$

$$\frac{dn_2^{\pm}}{dz} + id_2^{\pm} \omega n_2^{\pm} = \mp \alpha_2 n_2^{\pm} \pm g_1 P_2^{\pm} (n_1^{+} + n_1^{-}) \pm g_1 n_2^{\pm} (P_1^{+} + P_1^{-}) \mp g_2 \frac{\nu_2}{\nu_s} P_2^{\pm} n_s \mp g_2 \frac{\nu_2}{\nu_s} n_2^{\pm} P_s \pm \epsilon_2 n_2^{\mp} \quad (7)$$

$$\frac{dn_s}{dz} = -\alpha_s n_s + g_2 P_s (n_2^{+} + n_2^{-}) + g_2 n_s (P_2^{+} + P_2^{-}) + \epsilon_s n_s^{-} \quad (8)$$

$$\text{where } d_i^{\pm} = \frac{1}{\nu_s} \pm \frac{1}{\nu_i} \quad (9)$$

Where z is the length measured along the fiber span. The group velocity is described by  $\nu_i$ , referring to the wavelength of the pump for subscript “1”, first stokes for subscript “2”, or signal for subscript “s”. The attenuation coefficient,  $\alpha$ , is in units of  $\text{km}^{-1}$ . The optical frequency,  $\nu$ , refers to the first order pump, second order, or signal. The strength of the coupling between the pump and the signal is determined by g, the Raman gain efficiency of the

fiber which has units of  $(W \text{ Km})^{-1}$ . The pump modulation frequency is described by  $\omega$ . The signs  $\pm$  correspond to the pumps propagating in  $\pm z$  direction, meaning forward (+) and backward (-) propagating optical powers at the first order pump (1), second order pump (2) and signal (S). Here and through this paper is assumed that the signal propagates in the forward  $+z$  direction.  $\varepsilon$  are the Rayleigh backscattering coefficients of the fiber at each particular frequency. The two FBGs for the Stokes wavelength are located at  $z=0$  and  $z=L$  and have reflectivities  $R1$  and  $R2$  respectively. They are described by the two sets of boundary conditions:

For scheme 1

$$\begin{aligned} P_{P1}^+(0) = P_{10}^+, P_{P1}^-(L) = P_{10}^-, P_{P2}^+(0) = R_1 P_{P2}^-(0), P_{P2}^-(L) = R_2 P_{P2}^+(L), N_S^+(0) = N_0, N_S^-(L) = 0, P_S(0) = P_{IN} \\ n_1^+(0) = n_{10}, n_1^-(0) = n_{20}, n_2^+(0) = R_1 n_2^-(0), n_2^-(L) = R_2 n_2^+(L), n_S(0) = 0 \end{aligned} \quad (10)$$

For scheme 2

$$\begin{aligned} P_{P1}^+(0) = P_{10}^+, P_{P1}^-(L) = P_{10}^-, P_{P2}^+(0) = P_{20}^+, P_{P2}^-(L) = P_{20}^-, N_S^+(0) = N_0, N_S^-(L) = 0, P_S(0) = P_{IN} \\ n_1^+(0) = n_{10}, n_1^-(0) = n_{10}, n_2^+(0) = n_{20}, n_2^-(L) = n_{20}, n_S(0) = 0 \end{aligned} \quad (11)$$

The fiber parameters used in the simulation results for both systems, previously described by Figure 1 (a) and (b), are given in Table 1 and it corresponds to typical values for conventional SMF.

Table 1: Fiber parameters used in the simulation results

Wavelength (nm)	$g$ ( $W^{-1} \text{ km}^{-1}$ )	$\alpha$ (dB/km)	$\varepsilon$ ( $\text{km}^{-1}$ )
1365	0.51	0.33	$1.0 \times 10^{-5}$
1455	0.36	0.26	$6.0 \times 10^{-5}$
1550	-	0.2	$4.3 \times 10^{-5}$

Although the two sets of equations 1 - 5 and 6 - 8 describe a second order Raman amplification system, in principle there is no limit for applying a similar mathematical approach to higher order Raman amplification systems, at the cost of making the solution of the system substantially more complex.

### 3. Results and discussion

The solution of the numerical simulation described mathematically by the set of equations 1 to 8 can yield the impact of the span length, pump power distribution, FBGs reflectivity and type of fiber on the RIN transfer of the optical Raman amplifier system. As clarification, all the calculations for the numerical simulation work shown on this manuscript are conditioned to the quasi-lossless condition unless otherwise stated. The quasi-lossless condition aims to achieve the lowest power variation along the length of the fiber regardless the signal power, span length, pump power distribution or any other parameter of the amplifier system.

The numerical results for the RIN transfer value at several span lengths are shown on Figure 2. The results are graphically represented for the two amplifier systems described previously, Figure 2 (a) the ultra-long laser cavity

with 90% reflectivity FBGs and Figure 2 (b) the dual wavelength pumping scheme with no FBGs. The value of transmitted signal is 1mW in both cases. The initial RIN value of the laser pump is  $1\text{E-}9$ . The span length ranges from 1 to 100km. The only variable parameter is the length of the fiber span; otherwise the pump power distribution is symmetric and the quasi-lossless condition is satisfied.

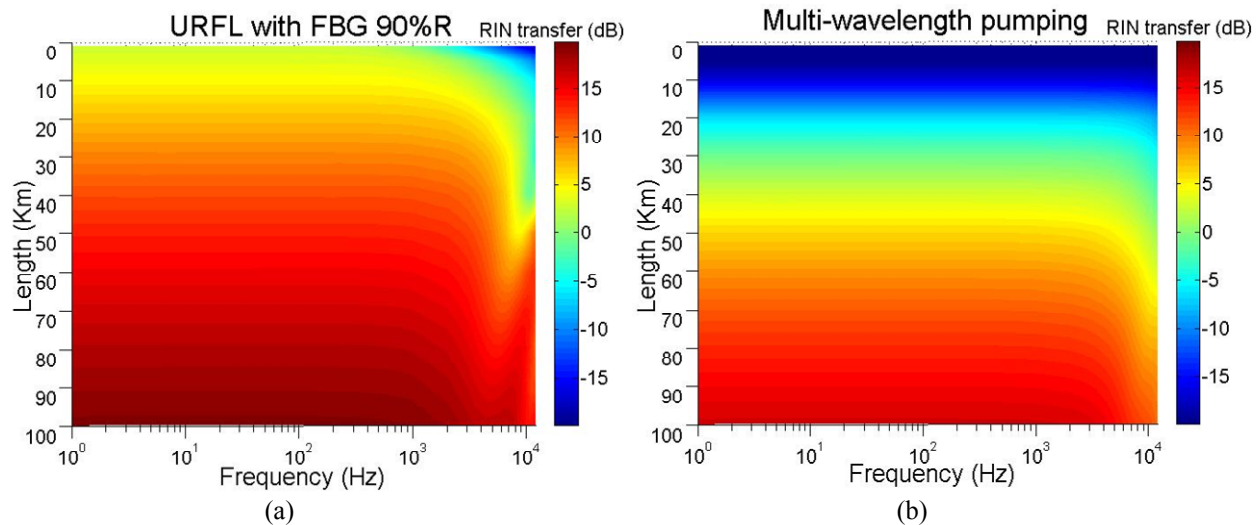


Figure 2: RIN transfer value at several span lengths for (a) laser cavity with 90% FBGs and (b) fiber span dual pumping scheme without reflectors

As a general trend, the maximum RIN transfer function value increases with length regardless of whether the Raman amplifier is a laser cavity or a second-order multi-wavelength pumped fiber span without reflectors. As an example, the maximum RIN value at 75km, for the cases of laser cavity with FBGs at 90% reflectivity and fiber span without reflectors, are 17dB and 12.25 dB respectively, i.e. RIN transfer is 4.75 dB higher in the ultra-long cavity configuration. Although the difference exists for all cases, it reduces as the span length increases, and for 100 km it is below 3.5 dB. A major difference between both systems results is the decline of the RIN transfer value at longer modulation frequencies. Whilst in the case of the dual pumping scheme without reflectors the RIN transfer drops gradually with increasing modulation frequency; in the case of the laser cavity the RIN transfer value shows a fluctuating behavior towards lower values, especially for the longer span lengths. Furthermore, as Figure 3 shows, the drop frequency, taken as 2dB lower than the maximum value, is lower for the laser cavity case than the fiber span without reflectors, given the same fiber length and power conditions. This cut-off frequency value is not fixed for all the span length cases.

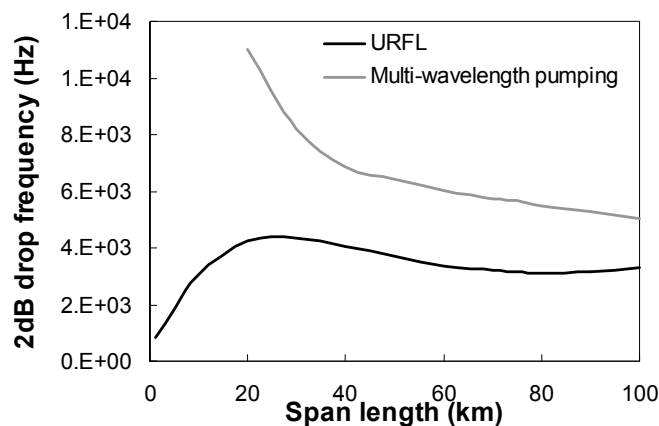


Figure 3: 2dB drop frequency versus span length. Comparison between two amplifier systems; a laser cavity with 90% reflectors and a fiber span dual pumping scheme without reflectors

The effect of the pump distribution is shown on Figure 4 for the cases of (a) laser cavity with 90% reflectivity FBGs and (b) dual wavelength pumping scheme without reflectors. The value of transmitted signal is again 1mW in both cases and the initial RIN of the laser pump is 1E-9. The span length is fixed at 75km. The pump ratio is calculated as the forward pump divided by the total amount of pump (forward and backward).

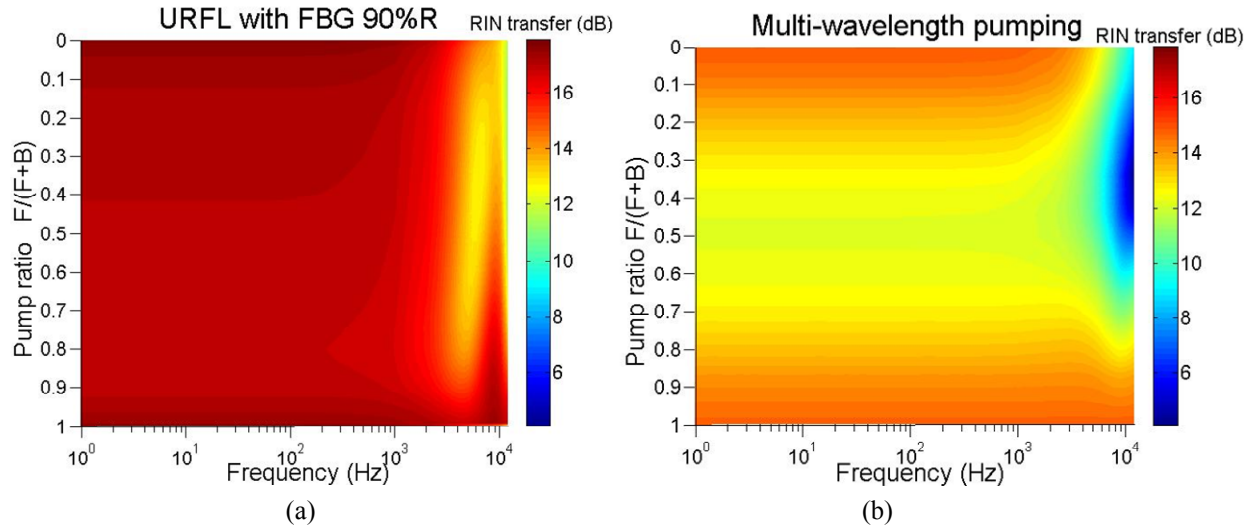


Figure 4: RIN transfer value for pumping distribution in the case of (a) 75km laser cavity with 90% reflectors and (b) 75km dual-wavelength second-order pumping scheme without reflectors.

The pump power distribution has a clear impact on the RIN transfer value. For the case of a laser cavity, Figure 4 (a) the optimum pumping distribution for the lowest RIN transfer value is 80% forward pump and 20% backward pump, with a value of 16.83dB. Using any pump power distribution other than 80% forward / 20% backward will have a relative low variation, maximum 0.9dB, on the RIN transfer value. The case of dual pumping scheme without reflectors, Figure 4 (b) shows symmetric pumping to be the best option, with a maximum RIN transfer value of 12.25dB. The variation of the RIN transfer value for any other pump distribution other than symmetric pumping can be up to 2.6dB for the conditions used on this work.

The profile of the RIN transfer value drops continuously for longer modulation frequencies in all the cases where the major pump contribution is from backward pumping (pump ratio towards 0). Forward pumping introduces a modulation of the RIN transfer value at longer frequencies, especially in the case of a laser cavity, displacing the drop frequency towards longer distances in the dual-wavelength pumping configuration. As we saw previously the drop frequency appears at shorter frequencies in the case of a laser cavity than the dual pumping scheme without reflectors, and therefore this modulation of the RIN transfer seems stronger for the case of laser cavity. For example, in a laser cavity case at 90% forward pump contribution, the peak fluctuation at longer modulation frequencies (i.e. 8.5kHz) is slightly higher, up to 0.8%, than at lower modulation frequency.

Figure 5 shows the RIN transfer values in a 75 km ultra-long laser cavity as grating reflectivity is varied 0.1% to 100%. As previously, these results were calculated using 1mW forward transmitted signal and 1E-9 as initial pump RIN value of the laser pump. The main result is that increasing FBGs reflectivity does not implies always the

highest value for RIN transfer; in fact the worst case is for relative low FBGs reflectivity, between 10 to 20% reflectivity.

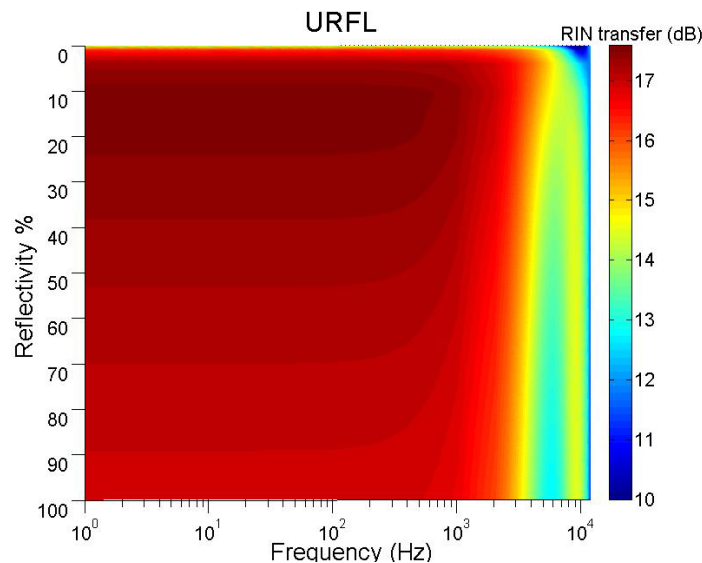


Figure 5: RIN transfer value for a 75km laser cavity for different FBG reflectivities.

As observed on the previous results, the 2 dB drop frequency is lower for higher reflectivities, with the worst case of RIN transfer taking place at 15% reflectivity at low modulation frequencies, and can be as low as to 5% for higher frequencies of the order of 6 kHz.

#### 4. Conclusion

We have described a numerical model for RIN transfer in higher order distributed Raman amplifiers, with special application to ultra-long Raman fiber lasers (URFL). This numerical model allows us a better understanding of how the design parameters of the laser cavity have an effect upon the RIN transfer performance of the system.

As expected the span length has a major impact on RIN transfer with an increasing RIN transfer value for longer lengths. At low modulation frequencies when transfer is usually highest, this RIN transfer value tends to converge towards a common value for long lengths, regardless of the rest of the design features of the Raman amplifier scheme. The maximum RIN transfer value is not linked to the highest reflectivity of the laser cavity, but in fact, happens at relative low reflectivity, 15%.

The pump ratio is a key parameter with effects in two aspects of the RIN transfer. On the one side it affects the maximum RIN transfer itself, although in different degrees depending of whether we are using a laser cavity or a dual-wavelength pumping scheme without reflectors. In addition, it also affects the modulation of the RIN transfer function at higher frequencies. This modulation is stronger at higher frequencies as the contribution of the forward pumping increases. A higher contribution of the backward pumping leads to a faster drop of the RIN transfer value with increasing frequency.

#### References

1. M. N. Islam, "Raman amplifiers for telecommunications", IEEE J. Select. Topics in Quantum Electron., 8 (3), pp. 548-559 (2002)

2. J. Bromage, "Raman amplification for fiber communications systems," J. of Lightwave Tech. 22(1) 79-93 (2004)
3. J.D. Ania-Castañón, T.J. Ellingham, R. Ibbotson, X. Chen, L. Zhang, S.K. Turitsyn, "Ultralong Raman Fiber Lasers as virtually lossless optical media," Phys. Rev. Lett. 96(2), 023902 (2006)
4. J.D. Ania-Castañón, Quasi-lossless transmission using second-order Raman amplification and fibre Bragg gratings," Opt. Express 12(9), pp. 4372-4377 (2004)
5. A.E. El-Taher, J.D. Ania-Castañón, V. Karalekas, P. Harper, "High efficiency supercontinuum generation using ultra-long Raman fiber cavities," Opt. Express 17(20), pp. 17909-17915 (2009)
6. M. Alcón-Camas, A.E. El-Taher, H. Wang, P. Harper, V. Karalekas, J.A. Harrison, J.D. Ania-Castañón, "Long-distance soliton transmission through ultralong fiber lasers," Opt. Lett. 34(20), pp. 3104-3106 (2009)
7. J. Scheuer, A. Yariv, "Giant fiber lasers: a new paradigm for secure key distribution," Phys. Rev. Lett. 97(14), 140502 (2006)
8. B. Bristiel, S. Jiang, P. Gallion, E. Pincemin, "New model of noise Figure and RIN transfer in fiber Raman amplifiers," IEEE Photo. Tech. Lett. 18(8), pp.980-982 (2006)