

Developing a New SVPWM Control Strategy for Open-Winding Brushless Doubly-Fed Reluctance Generators

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Abstract -- In this paper, a new open-winding control strategy is proposed for a brushless doubly-fed reluctance generator (BDFRG) used for standalone wind turbine or ship generators. The BDFRG is characterized with two windings on the stator: a power winding and a control winding. The control winding is fed with dual two-level three-phase converters, and a vector control scheme based on space vector pulse width modulation (SVPWM) is designed. Compared to traditional three-level inverter systems, the dc-link voltage and the voltage rating of power devices in the proposed system are reduced by 50% while still greatly improving the reliability, redundancy and fault tolerance of the proposed system by increasing the switching modes. Its performance is evaluated by simulation in MATLAB/SIMULINK, and an experimental study on a 42-kW prototype machine.

Index Terms--Brushless doubly-fed reluctance generator (BDFRG), dual two-level converters, open-winding, space vector pulse width modulation (SVPWM).

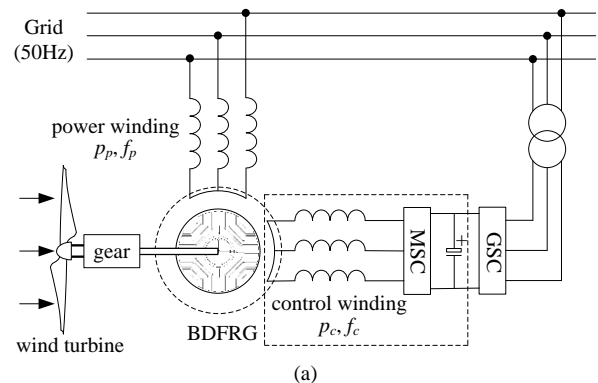
I. INTRODUCTION

The penetration of wind power into the power system is continuing to grow across the world [1]-[4], with an aid of rapid development of machine technologies, power electronics and automatic control.

The brushless doubly-fed machines are the evolution of the cascaded induction machine [5]-[13], and are widely used for medium and large wind turbines. Among them, brushless doubly-fed reluctance generators (BDFRGs) are a promising topology owing to their robust rotor [14]-[17]. As shown in Fig. 1(a), a typical BDFRG consists of two sets of stator windings: a power winding and a control winding. Since the rotor winding is moved to the stator as the control winding, the brushes and slip-rings in conventional doubly-fed machines are eliminated. Therefore the robustness and reliability is improved. However, the technical challenges lie in the rotor design where the double stator magnetic field

modulation is realized; and the control of the converters, which manipulates the flow of active and reactive power, and power factor regulation through power winding or the control winding [5]-[8]. The converters are of about 25% of the machine's rated power to control a wide speed range at various operating modes including super-synchronous, synchronous and sub-synchronous. Compared with the doubly-fed induction machine and permanent magnet synchronous machine, the BDFRG is better suited for wind turbines, shaft generators, pumps, and hydropower generation systems [9]-[17].

In references [5]-[18], a BDFRG and its power generation systems were analyzed by scalar control, vector control, and the power flow analysis. It is well known that traditional three-level converter systems have some disadvantages [19], [20], such as complex structure, high voltage of DC link and power devices, and the potential shift of neutral point voltage. In order to improve these, some variable-speed constant-frequency (VSCF) schemes were proposed [12]-[17], [21]-[23]. As shown in Fig. 1(b), where have some obvious advantages compared with the previous generator system, i.e., the control winding of the BDFRG is open-circuited and fed with dual two-level converters, and the space vector pulse width modulation (SVPWM) coordination control strategy is adopted, then the reliability, redundancy and fault tolerance of the proposed system are greatly improved while the dc-link voltage and the voltage rating of power devices are reduced by 50%.



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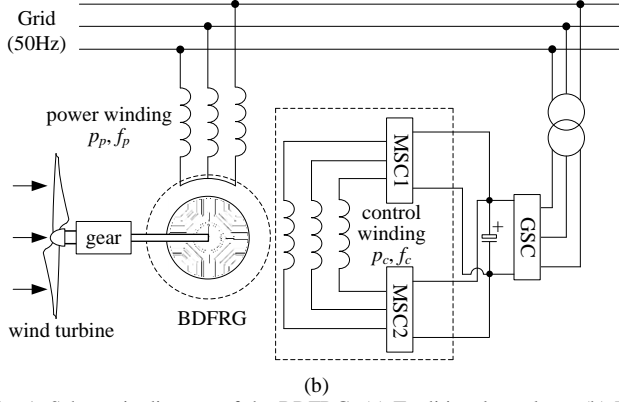


Fig. 1. Schematic diagram of the BDFRG. (a) Traditional topology, (b) The proposed topology.

II. OPEN-WINDING CONTROL STRATEGY OF BRUSHLESS DOUBLY-FED GENERATOR

A. The Principle of VSCF Based on BDFRG

The BDFRG is a new type of machine developed in recent years [7]; its stator has two sets of stator windings with two different pole numbers. The primary winding (also known as the power winding) is directly connected to the grid and the secondary winding (also known as the control winding) is fed through the converter, as shown in Fig. 1. The relationship between frequency, pole pairs and operating speed of the BDFRG is given by:

$$f_p = \frac{n_r (p_p + p_c)}{60} \pm f_c \quad (1)$$

where f_p is the supplied line frequency (also known as the frequency of power winding); n_r is the rotor speed in rpm; p_p and p_c are the pole pair of the power and control windings, respectively; f_c is the converter frequency (also known as the frequency of control winding).

Obviously, the BDFRG is suited for VSCF operations and its application includes wind turbines, shaft generators and hydroelectric generators.

B. Mathematical Model of BDFRG

For control implementation, the voltage balance equation in a rotating reference frame [8] is expressed as (2), and the flux equations is expressed as (3),

$$\begin{cases} u_{qp} = r_p i_{qp} + p(L_p i_{qp} - L_{pc} i_{qp}) + p[L_{pc}(i_{qp} - i_{qc})] + \omega \psi_{dp} \\ u_{dp} = r_p i_{dp} + p(L_p i_{dp} - L_{pc} i_{dp}) + p[L_{pc}(i_{dp} + i_{dc})] - \omega \psi_{qp} \\ u_{qc} = r_c i_{qc} + p(L_c i_{qc} - L_{pc} i_{qc}) + p[L_{pc}(i_{qc} - i_{qp})] + (\omega_r - \omega) \psi_{dc} \\ u_{dc} = r_c i_{dc} + p(L_c i_{dc} - L_{pc} i_{dc}) + p[L_{pc}(i_{dc} + i_{dp})] - (\omega_r - \omega) \psi_{qc} \end{cases} \quad (2)$$

$$\begin{cases} \Psi_{qp} = L_p i_{qp} - L_{pc} i_{qc} \\ \Psi_{dp} = L_p i_{dp} + L_{pc} i_{dc} \\ \Psi_{qc} = L_c i_{qc} - L_{pc} i_{qp} \\ \Psi_{dc} = L_c i_{dc} + L_{pc} i_{dp} \end{cases} \quad (3)$$

where the letter “ p ” denotes the differential operator, the subscripts “ d ” and “ q ” denote the d -axis and q -axis components; “ p ”, “ c ” and “ r ” denote the power winding, control winding and rotor components, respectively. ω is the speed of the rotating coordinate system, ω_r denotes the rotor angular speed, L_{pc} is the mutual inductance between power and control winding.

The electromagnetic torque is expressed as (4) and (5) [11],

$$T_{em} = \frac{3(p_p + p_c)L_p}{2(L_p L_c - L_{pc}^2)} |\Psi_p| |\Psi_{pc}| \sin \delta \quad (4)$$

$$T_{em} - T_L - K_d \dot{\varpi}_r = J \frac{d\varpi_r}{dt} \quad (5)$$

where Ψ_p and Ψ_{pc} denote the flux linkage of power winding and mutual flux linkage between power and control winding, and δ is the angle between them. T_{em} denotes the total electromagnetic torque, T_L denotes the load torque, J denotes the moment of inertia, K_d denotes the rotary system damping coefficient.

C. The Control Strategy of BDFRG

Also in Fig. 1, the wind turbine will drive the rotor to rotate, where the power winding is directly connected to the grid or load, and the control winding is connected between two bi-directional converters and then to the grid. During an operation, the control winding is fed with the machine side converter (MSCs) supplied by the grid side converter (GSC) to generate a magnetic field. When the BDFRG is driven by the wind turbine, power is generated for the grid, load, or charging the battery. In Fig. 1(b), the dotted box represents a control topology for the dual two-level converters, which is further shown in detail in Fig. 2, where the control winding is open-circuited (thus the machine is termed the open-winding BDFRG, OWBDFRG), and fed with two reversible converters (MSC1 and MSC2) supplied by one DC bus and by combining dual two-level converters, can form a three-level converter while the DC bus voltage ($U_{dc}/2$) is only half of traditional three-level converter (U_{dc}) [19]-[20], as shown in Fig. 3. That is, by using the open-winding control strategy, the capacitance of the DC-link and the voltage rating of power devices can be decreased. When compared with typical two-level converters, the open-winding control strategy increases the converter voltage step level so that the switching power losses are also reduced. If one of the two MSCs is faulted or disconnected, the system can still operate with the remaining MSC.

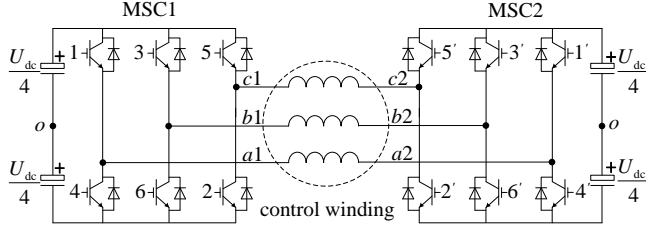


Fig. 2. The system diagrams of the OWBDFRG.

For the OWBDFRG shown in Fig. 2, the instantaneous voltages of the control winding can be found as (6), (7).

$$\begin{cases} u_{ca} = u_{a10} - u_{a20} = u_{a1a2} \\ u_{cb} = u_{b10} - u_{b20} = u_{b1b2} \\ u_{cc} = u_{c10} - u_{c20} = u_{c1c2} \end{cases} \quad (6)$$

$$u_c = u_{MSC1} - u_{MSC2} \quad (7)$$

D. SVPWM Coordination Control Strategy

The SVPWM control strategy, also called the flux sine PWM control, uses the output voltage of the three-phase inverter in different switching modes to approach to the inscribed circle of the corresponding regular polygon, then the sine round rotating magnetic field is obtained with a constant amplitude in the machine, the advantages of SVPWM and constant flux control can be realized.

In Fig. 2, the phasor diagram of two-level converter (MSC1, MSC2) is shown in Fig. 4, where the hexagon vertex respectively to 1-6 and 1'-6', and the space is divided into six sectors, the effective voltage space vector is U_1-U_6 and $U_1'-U_6'$ (1-6 and 1'-6', respectively), which the mode is $U_{dc}/3$, zero vector is of U_7, U_8, U_7' and U_8' (7, 8, 7' and 8', respectively). Traditionally, the maximum switching mode is $2^3=8$ in a two-level three-phase converter and $3^3=27$ in a three-level converter [19]-[23], as shown in Fig. 3. By cascading the dual two-level converters (see Fig. 2), the switch modes in the proposed converter can increase to $2^3 \times 2^3 = 64$ (see Fig. 5(a)). Obviously, the redundancy and fault tolerance of the proposed topology are improved.

The diagram of the voltage space vector with a dual two-level converter is shown in Fig. 5 (a), where the synthesis 64 voltage space vector is 11'-88'. The control space is divided into 24 small sectors or one inner hexagon and six outer hexagons, i.e., ABCDEF is the inner hexagon with its center of O, six outer hexagons are OFSGHB, OAHJIC, OBJKLD, OCLMNE, ODN PQF and OEQRSA, with their midpoints of A-F. In this paper, the two reference voltage space vectors are chosen for the two converters (MSC1, MSC2).

$$\begin{cases} U_{MSC1} = \frac{1}{2} U_{ref} \\ U_{MSC2} = -\frac{1}{2} U_{ref} \end{cases} \quad (8)$$

U_{MSC1} , U_{MSC2} and U_{ref} denotes the voltage vector of MSC1, MSC2 and the reference voltage of the control winding, respectively, as shown in Fig. 5(b).

It is needed to make sure that the two voltage vectors have the same amplitude as the reference voltage phasor (half of the reference voltage vector).

Assuming that the reference voltage vector U_{ref} lies in $\triangle IOG$, as shown in Fig. 5(b), corresponding to Fig. 4(a) which lies in sector 1 for MSC1, and (b) lies in sector 4 for MSC2.

In Fig. 4(a), due to the parallelogram law, the reference voltage vector U_{MSC1} consists of two adjacent effective vectors U_1, U_2 , and zero vector U_0 , and the operating time can be calculated [22], [23].

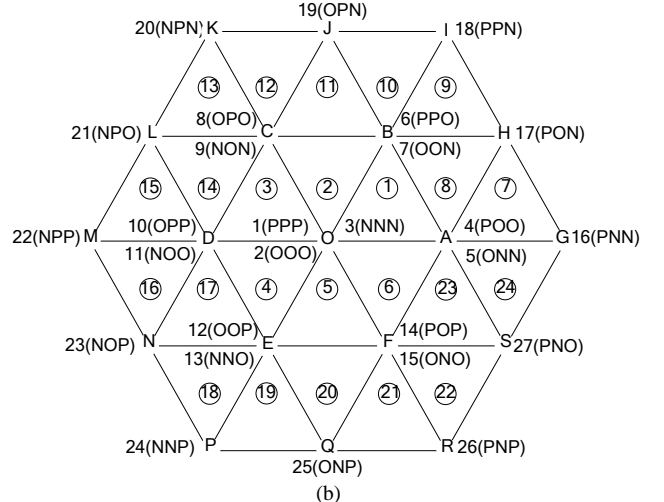
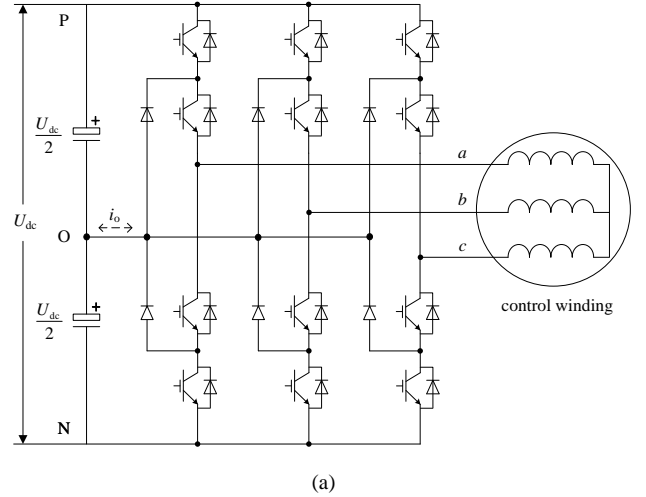


Fig. 3 Topology of BDFRG fed by NPC three-level converter. (a) Topology, (b) Voltage space vector.

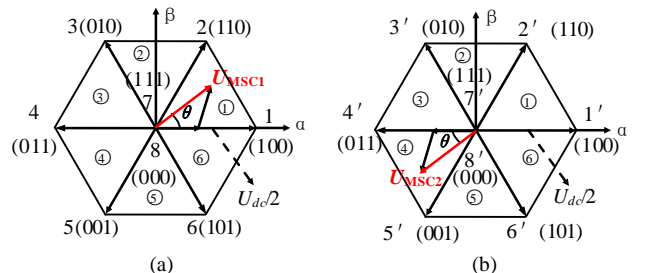


Fig. 4. The space phasors in each inverter. (a) MSC1, (b) MSC2.

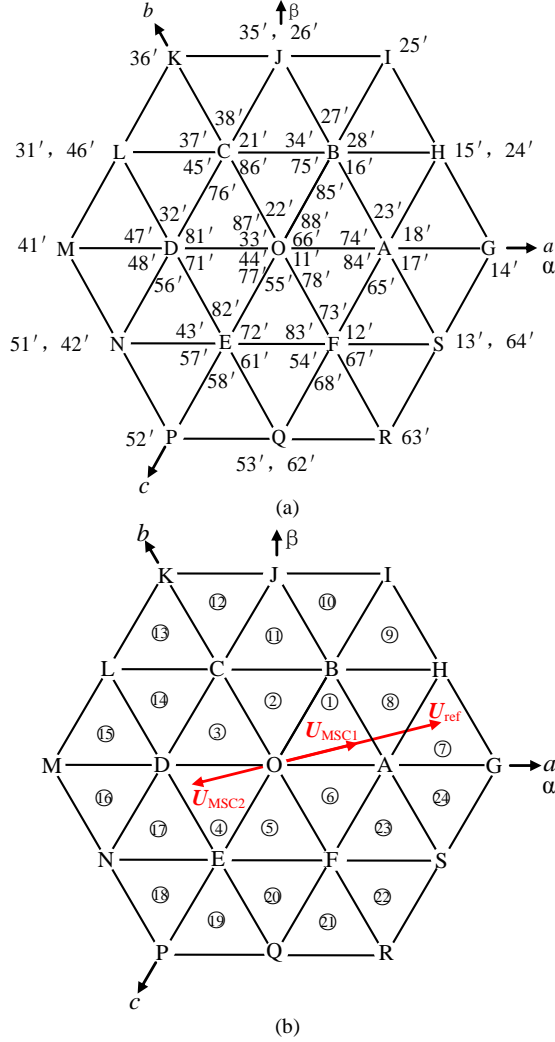


Fig. 5. The space phasors of proposed dual two-level converters. (a) Voltage phasors, (b) Relationship between MSC1, MSC2 and reference voltage vector.

III. SIMULATION RESEARCH ON THE CONTROL STRATEGY

A. The Simulation Model of the Control System

The simulation model of the proposed system is established in MATLAB/SIMULINK, as shown in Fig. 6, where includes a OWBDFRG, a resistive load, a reference speed n_r^* , frequency calculation (f_c), static three-phase coordinates/rotary two-phase coordinates transformation ($3s/2r$), rotary two-phase coordinates/static two-phase coordinates transformation ($2r/2s$), control strategy of constant voltage frequency ratio (U/f), the SVPWM scheme.

During the operation, according to the reference speed n_r^* of generator rotor, and line frequency of 50 Hz, the required frequency and voltage of control winding is calculated in real-time, i.e., by the machine side dual two-level converters with SVPWM coordinated control, then the voltage and frequency required by the dual MSCs can be generated.

B. Analysis of Simulation Results

The generator parameters as: $P_N=42\text{kW}$, $U_{N,p}=U_{N,c}=380\text{V}$, $p_p=3$, $R_p=0.1662\ \Omega$, $L_p=0.01737\ \text{H}$, $L_{pc}=0.01813\ \text{H}$, $p_c=1$, $R_c=0.1882\ \Omega$, $L_c=0.02351\ \text{H}$, $J=0.3\ \text{kg.m}^2$.

In order to validate the effectiveness of the proposed topology in VSCF, the simulation is firstly carried out at the speed of 606, 750, and 789 rpm, corresponding to sub-synchronous, synchronous, and super-synchronous modes of the BDFRG. Simulation results are shown in Figs. 7-10. Fig. 7 shows the voltage reference in phase a of the control winding according to the VSCF generation, Figs. 8-10 show the phase voltage, line voltage and current of the control winding, respectively. As can be seen from these figures, the proposed SVPWM three-level control strategy in open-winding brushless doubly-fed reluctance generator is effective.

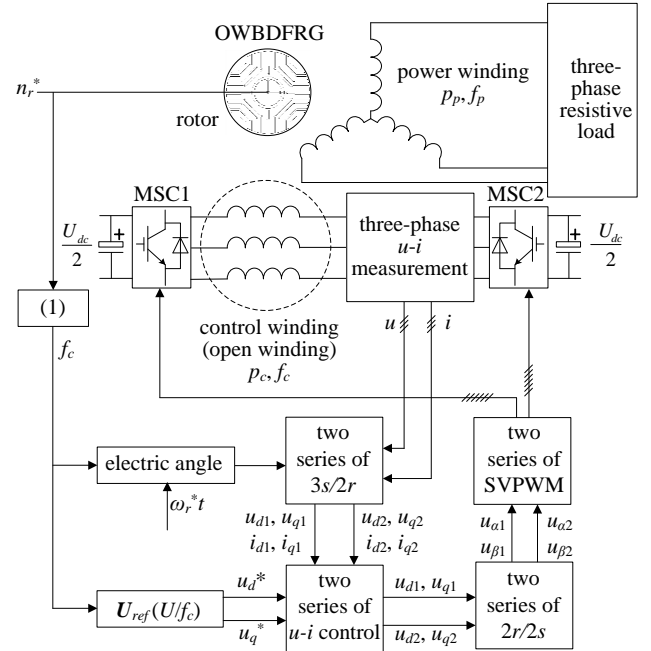
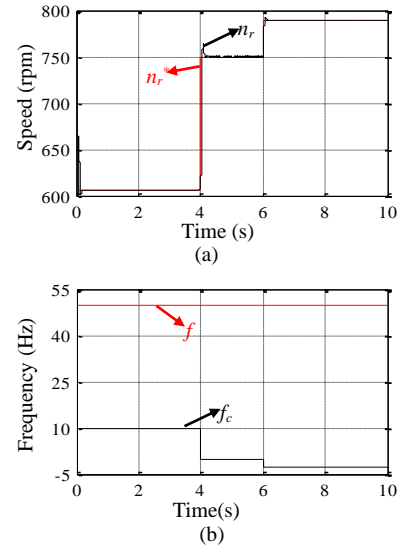


Fig. 6. The simulation diagram of the proposed control scheme.



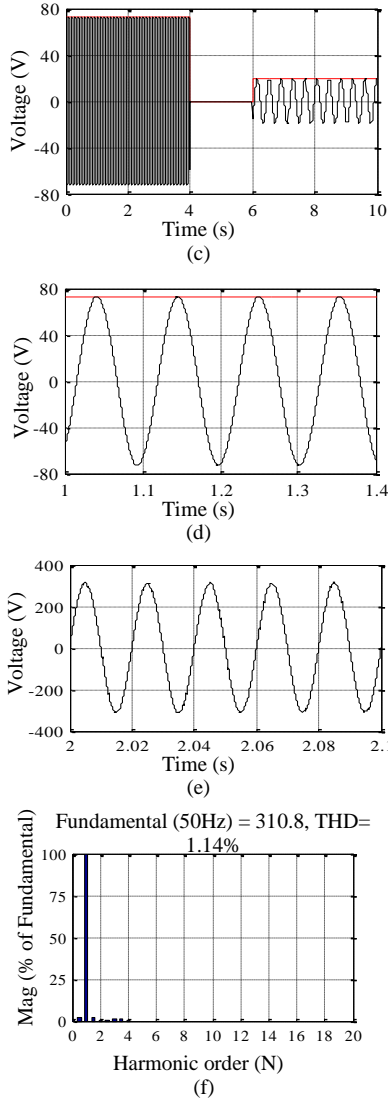


Fig. 7. Simulation results in PW, CW. (a) n_r^* , n_r , (b) stator frequency of PW, CW, (c) reference voltage of control winding, u_{carefs} , (d) enlarged vision of (c), (e) voltage of power winding in phase a , u_{pa} , (f) FFT analysis of u_{pa} .

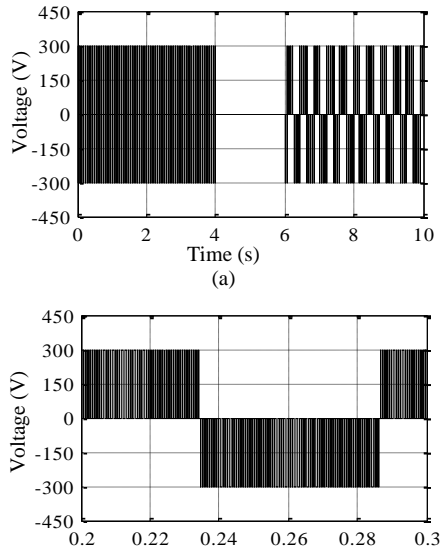
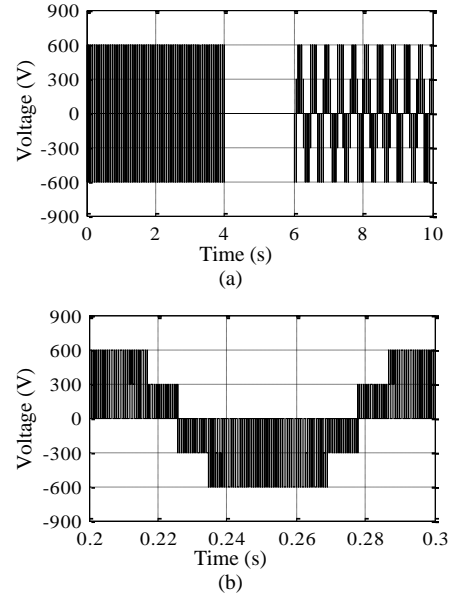


Fig. 8. The voltage waveform in phase a of control winding, (a) full speed range, (b) sub-synchronous (606 rpm), (c) enlarged vision of (b), (d) super-synchronous (789 rpm), (e) enlarged vision of (d).



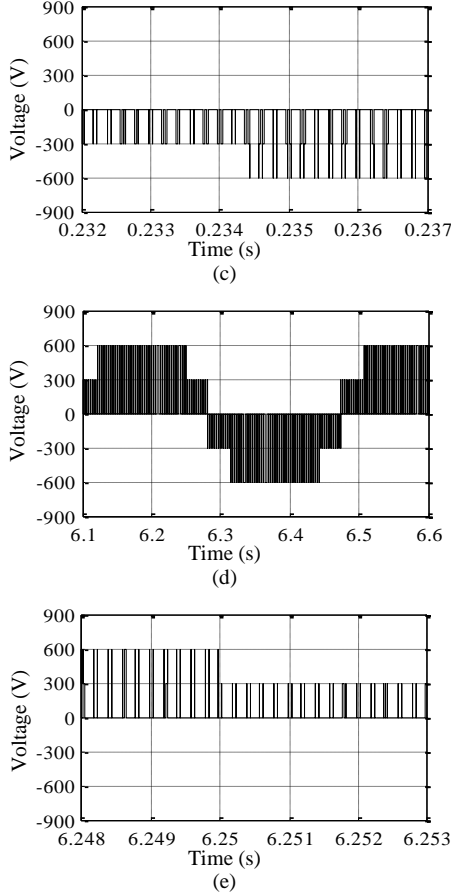


Fig. 9. The line voltage waveform between phase *a* and *b* of control winding. (a) full speed range, (b) sub-synchronous (606 rpm), (c) enlarged vision of (b), (d) super-synchronous (789 rpm), (e) enlarged vision of (d).

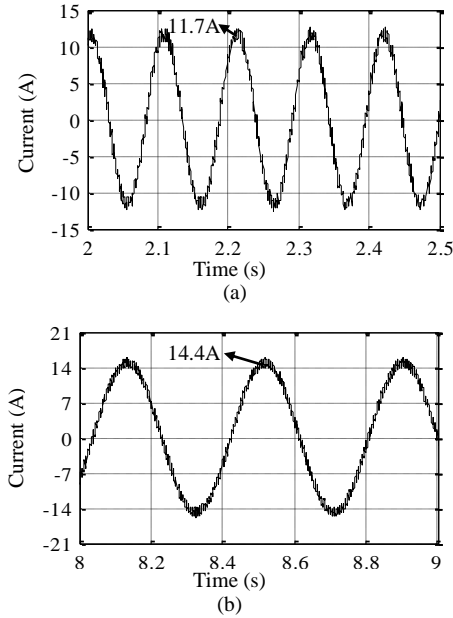


Fig. 10. The current in phase *a* of control winding. (a) Sub-synchronous (606 rpm). (b) Super-synchronous (789 rpm).

IV. EXPERIMENTAL RESULTS

The proposed control strategy is implemented and executed in DSP28335 in a semi-physical simulation experimental platform as shown in Fig. 11, where includes a prime mover of the induction motor (IM), OWBDFRG, resistive load, converter (15 kW), power analyzer, thermal imager, and so on.

The experimental results in the sub-synchronous and super-synchronous modes ($n_r^* = 606$ and 789 rpm, respectively) are shown in Figs. 12-15. Figs. 12-13 present the control winding voltage waveforms, where Fig. 12-13(a) and (c) are the voltage in phase *a* and line voltage between phase *a* and *b*, Figs. 12-13(c), (d) are their enlarged visions, which are all corresponding to Fig. 8-9, and are same to the voltage of traditional three-level converter. Fig. 14 shows the current in phase *a* of control winding, which also corresponds to Fig. 10.

Fig. 15(a)-(b) demonstrates the power winding voltage in phase *a* and its Fourier analysis result. The phase voltage is about 224 V, 50 Hz, the THD is 3.7%, and the third harmonic voltage is 4.747 V, which satisfying the VSCF requirements.

From the above analysis of experimental results as shown in Fig. 12-15, we can obtain that the new SVPWM strategy of proposed OWBDFRG fed with dual two-level converters is correct and valid, the control effectiveness and feature are the same to the traditional three-level converter, which is of three-level phase voltage and five-level line voltage, while the dc bus voltage is lower than three-level converter, the reliability, redundancy and fault tolerance of the proposed system are greatly improved, but does not have the traditional three-level converter disadvantages, such as complex topology, potential deviation of neutral point, and so forth.

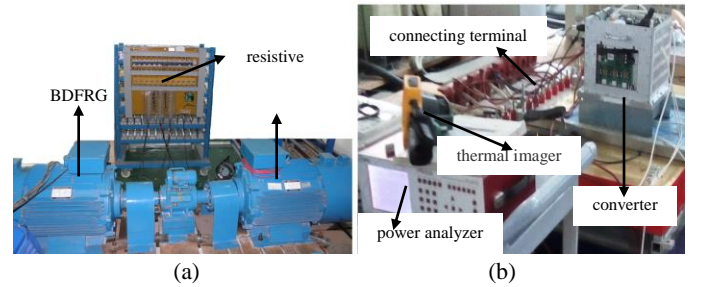
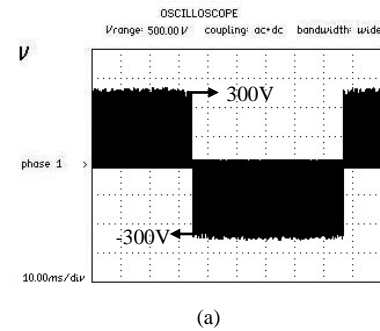
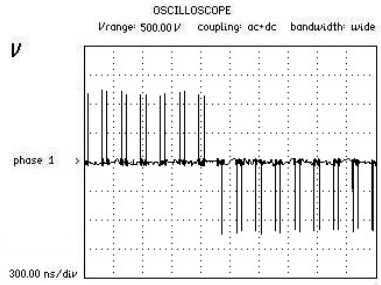


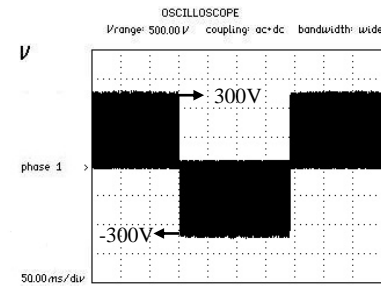
Fig. 11. The semi-physical simulation experimental platform. (a) The BDFRG, IM and resistive load, (b) The converter.



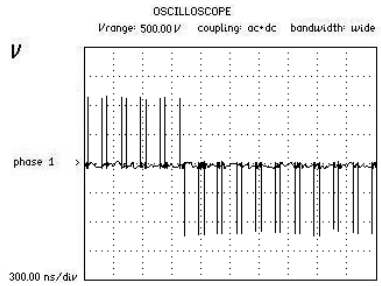
(a)



(b)

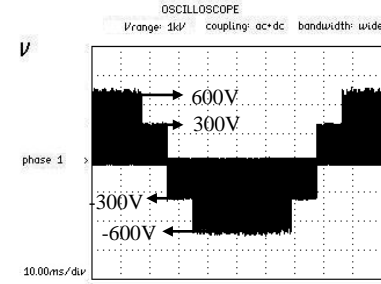


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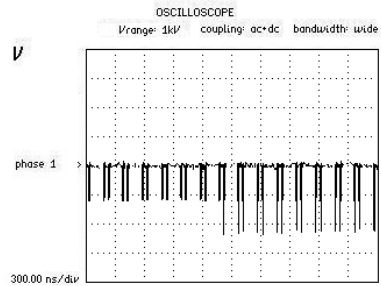


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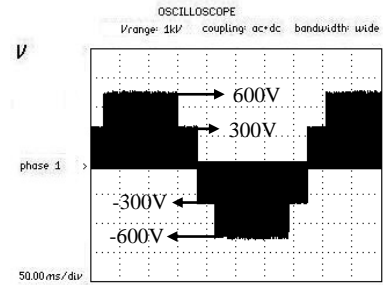
Fig. 12. The voltage waveform in phase a of control winding. (a) sub-synchronous (606 rpm), (b) super-synchronous (789 rpm).



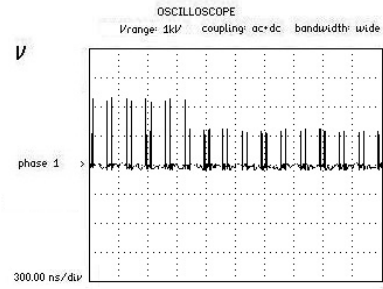
(a)



(b)

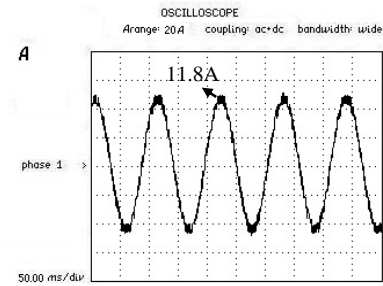


(c)

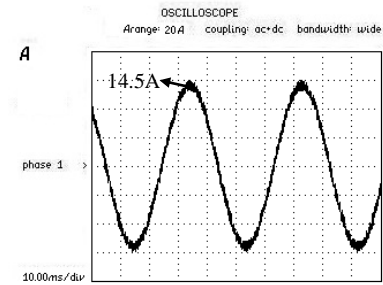


(d)

Fig. 13. The line voltage between phase a and b of control winding. (a) sub-synchronous (606 rpm), (b) super-synchronous (789 rpm).

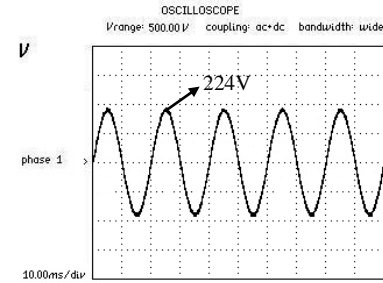


(a)



(b)

Fig. 14. Phase current in the control winding. (a) Sub-synchronous (606 rpm), (b) Super-synchronous (789 rpm).



(a)

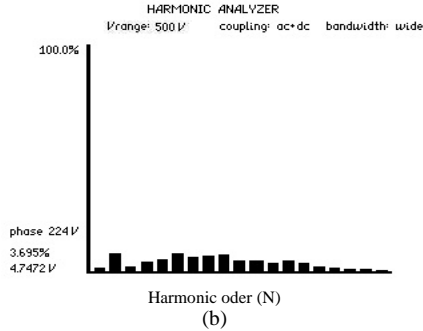


Fig. 15. Phase voltage of the power winding and its Fourier analysis. (a) Power winding voltage in phase a, (b) Fourier analysis result.

V. CONCLUSION

This paper has presented a novel control strategy for the OWBDFRG, based on the dual SVPWM coordinate control. The validity of the proposed algorithm is proved by simulation and experimental tests, and the advantages of the proposed strategy are a simpler main circuit structure, more convenient control scheme, lower DC-link voltage and the power device rating while achieving higher redundancy and better fault tolerance than existing conventional BDFRG control schemes. It will improve the performance of wind turbine or hydropower generators.

In the further work, a grid-connected control strategy will be developed to extend the application of the BDFRG.

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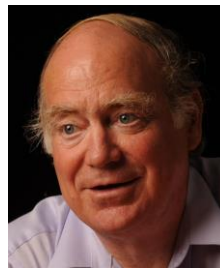
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