

**An ultrasensitive and universal surface plasmonic biosensor for
detection of micropollutants in aquatic environments**

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ABSTRACT

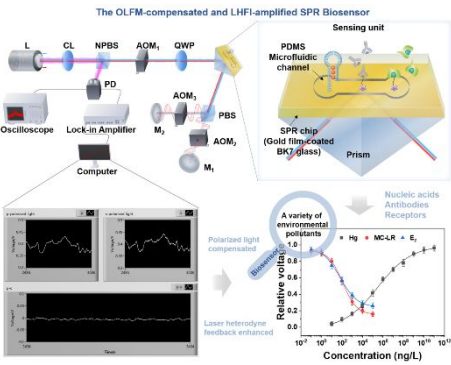
Simple and yet ultrasensitive and accurate quantifying a variety of analytical targets by virtue of a universal sensing device holds promise to revolutionize environmental monitoring, medical diagnostics, and food safety. Here, we propose a novel optical surface plasmon resonance (SPR) system in which the frequency-shifted light of different polarization returned the laser cavity to stimulating laser heterodyne feedback interferometry (LHFI), hence amplifying the reflectivity change caused by the refractive index (RI) variations on the gold-coated SPR chip surface. In addition, the *s*-polarized light further used as the reference to compensate the noise of the LHFI-amplified SPR system, resulting in nearly 3 orders of magnitude enhancement of RI resolution (5.9×10^{-8} RIU) over the original SPR system (2.0×10^{-5} RIU). By exploiting nucleic acids, antibodies, and receptors as recognition materials, a variety of micropollutants are detected with ultra-low detection limits, ranging from a toxic metal ion (Hg^{2+} , 70 ng/L), to a group of commonly occurring biotoxin (microcystins, 3.9 ng microcystin-LR/L), and to a class of environmental endocrine disruptors (estrogens, 0.7 ng 17β -estradiol/L). This sensing platform exhibits several distinct characteristics, including dual improvement of sensitivity and stability, and common-path optical construction without needing optical alignment, demonstrating a promising avenue towards environmental monitoring.

KEYWORDS

Environmental monitoring; Surface plasmon resonance; Laser heterodyne feedback; Polarized light compensation; Biosensor; Ultrasensitive detection

36 **SYNOPSIS**

37 An OLFM-compensated and LHFI-amplified SPR biosensor for ultrasensitive detection
38 of a variety of analytical targets with universality.



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For TOC

42 INTRODUCTION

43 Precise and reliable monitoring micropollutants of widespread concern in aquatic
44 environment, is of great significance for the risk assessments of public safety and
45 ecological health. Traditional analytical devices, such as high-performance liquid
46 chromatography (HPLC), and gas chromatography–mass spectrometry (GC–MS), are
47 greatly limited in sensitivity and universality, especially compounds that have not been
48 previously recognized. Therefore, developing a universal biosensing platform with
49 excellent sensitivity and stability, to quantify and assess a broad range of analytical
50 targets is in high demand for environmental monitoring.

51 Significant advances have been witnessed in the use of various biological recognition
52 material-based schemes to detect analytical targets, such as antibodies,¹ functional
53 nucleic acids,² and receptors³ recent years. Among these, one of the most successful and
54 commonly used schemes is refractive index (RI)-based label-free optical biosensing and
55 the biosensors developed therefrom have been exploited for a broad range of
56 applications due to their excellent performance, such as easy-to-operation and showing
57 enormous potential for miniaturization and for simultaneous quantification of
58 multiplexed analytical targets.⁴ Surface plasmons are electromagnetic excitations that
59 propagate along an interface between metal and dielectric medium, consisting of an
60 interface-bound evanescent wave in the dielectric and medium charge density
61 oscillations in the metal.⁵ As a typical RI-based label-free optical biosensor,
62 conventional intensity-modulated surface plasmon resonance (SPR) system based on
63 prism coupling has been widely reported, generally exhibiting a RI resolution of 10^{-5}

64 RIU.⁶

65 Although various sensitivity enhancement schemes have been exploited building on the
66 basic structure of SPR, such as optimizing the SPR-coated layer,⁷ utilizing phase or
67 angular modulation,⁸ and adding a nanodielectric layer,⁹ they have trade-offs among
68 sensitivity, simplicity, stability, and cost. As an alternative, the laser heterodyne
69 feedback interferometry (LHFI) makes the feedback weak optical signal participate in
70 the stimulated radiation of the laser for spontaneous amplification, that can be leveraged
71 for intensity-modulated SPR sensitivity enhancement. More specifically, the frequency-
72 shifted incident light senses, and then partially returns to the laser cavity, in turn
73 resonating with the relaxation oscillation and inducing the intensity modulation of the
74 laser; as a consequence, the modulated output of the laser can be enhanced even up to
75 10^6 -fold compared with the feedback one.^{10, 11} In this scheme, the laser source acts as an
76 emitter, responder, and intrinsic amplifier simultaneously, which does rarely need
77 optical alignment and reduces optical components required. Because of its compactness,
78 self-collimation, and sensitivity, the LHFI has been widely explored for displacement
79 sensing,¹² particle detection,¹³ confocal tomography¹⁴ and so on. Despite of its promise,
80 enhanced sensitivity to SPR via the LHFI is rarely reported so far. Besides, the inherent
81 noise caused by the air disturbance and the laser is an unavoidable problem in the label-
82 free SPR sensing.

83 To address the challenge, we exploited a polarized light-compensated SPR system with
84 laser heterodyne feedback for ultrasensitive detection of a various of analytical targets.
85 In this platform, the LHFI was adopted to remarkably amplify the intensity change

caused by the molecular/biomolecular binding-induced RI variations when the SPR was excited on the surface. Inspired by the common-path compensation reports via frequency multiplexing¹⁵ or polarized light,¹⁶ we further proposed a common-path compensation approach combining the orthogonally-polarized light with frequency multiplexing (OLFM) to minimize the impact of mechanical, thermal, and laser noise, which was compatible with the SPR system and significantly improved the stability of this system. Subsequently, the strategy to anchor functional groups/molecules on the SPR chip was realized by forming self-assembled monolayers (SAMs) spontaneously on gold film via the Au-S bond. As proof-of-concept demonstrations, we adopted this technique for specifically detecting mercury ions (II) (Hg^{2+}), broad-spectrum immunoassay of microcystins (MCs), and screening of estrogenic binding activity in environmental samples and achieved ultralow detection limits.

MATERIALS AND METHODS

Experimental Procedures

Detailed information on materials and reagents were provided in the Supporting Information (**Note S1**).

Experimental setup. The OLFM-compensated and LHFI-amplified SPR system was excited by using a home-made 1064 nm solid-state microchip laser. The incident angle was controlled via an electric turntable (Micronix Inc., PR-50-11300) attached to the sensing unit with a resolution of 5 microdegrees and a scanning range from 0 to 360 degrees. The sensing unit of this system was composed of a microfluidic channel (9×6 mm in area and 1 mm in depth) made of polydimethylsiloxane (PDMS) and a SPR chip

on the prism (Daheng Optics Inc., GCL-030102A). The SPR chip was made of a BK7 glass slide (20×20 mm in area and 1 mm in depth) coated with 2 nm chromium adhesion layer and 52 nm gold film by using an electron-beam evaporator (Canon-Anelva Inc., L-400EK). The *p*- and *s*-polarized beams were frequency shifted by three AOMs (Castech Inc., CAFS-70-3-020-TEC-1064-AF). The modulated light was acquired by using a PD (Thorlabs Inc., PDA20CS2) with a lock-in amplifier (Zurich Instrument Inc., HF2LI). Different samples were injected in the microfluidic channel at a constant flow velocity of 100 μ L/min by a syringe pump (Longer Inc., LSP01-2A). The SPR signal responses during the detection process were ultimately acquired by using a PD with a lock-in amplifier and recorded online and in real-time by LabView software.

Statistical Information. Statistical analysis was performed using Origin 2022. The four-parameter logistic model with unfixed lower and upper boundaries was adopted for curve-fitting. Error bars in all figures represent the standard deviations of three individual experiments in parallel and the blue dotted lines represent the 95% confidence band.

RESULTS AND DISCUSSION

OLFM-compensated and LHFI-amplified SPR Detection Principle. To achieve the sensitivity and stability enhancement to SPR, we designed a novel optical structure in which the frequency-shifted light of different polarization returned to the laser cavity to stimulate LHFI and the *s*-polarized light used as the reference to compensate the noise of the LHFI-amplified SPR system (**Figure 1a** and **Figure S1**). More specifically, the output light of the laser was separated into two parts by a non-polarized beam splitter

(NPBS). The transmitted beam was adjusted to circularly polarized light by a quarter-wave plate (QWP) and then incident on the gold film of the SPR chip. After passing through the sensing unit, the circularly polarized light was divided into p - and s -polarized light by a polarized beam splitter (PBS). Both of them were frequency shifted differently and reflected by two mirrors (M_1 and M_2), respectively. The feedback beams returned to the laser cavity along the original path, hence inducing the intensity modulation of the laser. The modulated laser power output caused by the two feedback beams can be described as:^{17, 18}

$$\frac{\Delta I_p(\Omega_p)}{I} = \kappa_p G(\Omega_p) \cos(2\pi\Omega_p t - \phi_{fp} + \phi_{ep})$$

$$\frac{\Delta I_s(\Omega_s)}{I} = \kappa_s G(\Omega_s) \cos(2\pi\Omega_s t - \phi_{fs} + \phi_{es})$$

where ΔI_p and ΔI_s are the feedback light-induced intensity modulation of p -polarized beam and s -polarized beam, respectively; Ω_p and Ω_s are the shift frequencies of the two beams; I denotes the stationary laser intensity; κ_p and κ_s are the coefficients of the feedback strength of the two beams; ϕ_{fp} and ϕ_{fs} are the fixed phases of the two beams; ϕ_{ep} and ϕ_{es} are the external phases of the two beams; $G(\Omega_p)$ and $G(\Omega_s)$ are the frequency-dependent gain factors. To compensate the intensity drift induced by air disturbance, laser and other inherent mechanical and thermal noise, we defined $\Delta I = \Delta I_p - \Delta I_s$ as the corrected intensity change corresponding to the RI variations. The light intensity was ultimately acquired by using a photodiode (PD) with a lock-in amplifier and recorded in the form of voltage by a computer.

To obtain a larger gain factor $G(\Omega_i)$ and demodulate the p - and s -polarized beams

separately, three acousto-optic modulators (AOMs) were employed, in which AOM₂ and AOM₃ were set with different working frequencies (**Figure 1b**). The frequency-dependent gain factor $G(\Omega_i)$ can be expressed as:^{18, 19}

$$G(\Omega_i) = 2\gamma_c \frac{(\eta^2\gamma^2 + 4\pi^2\Omega_i^2)^{1/2}}{[4\eta^2\gamma^2\pi^2\Omega_i^2 + (4\pi^2f_r^2 - 4\pi^2\Omega_i^2)^2]^{1/2}}$$

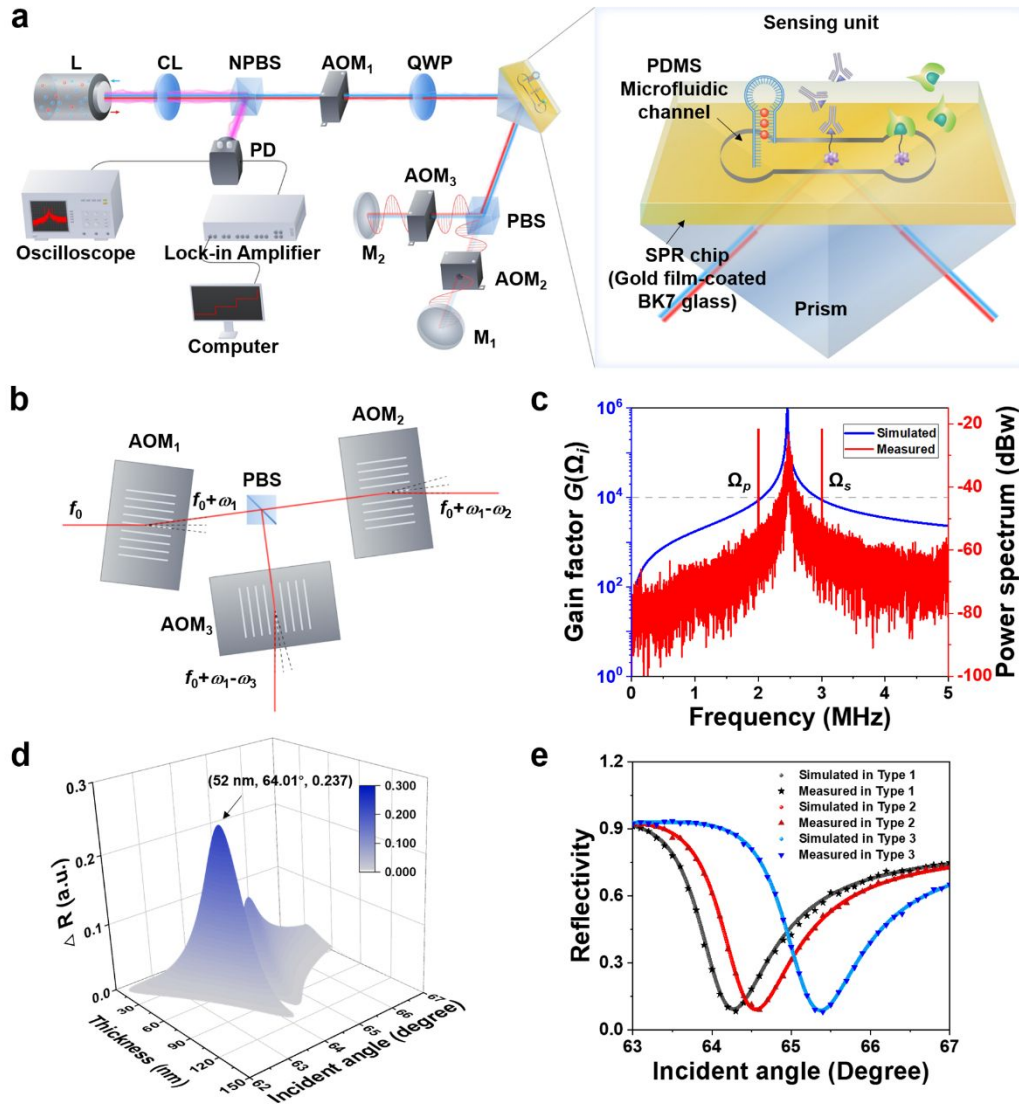
where γ_c is the photon decay rate inside the laser cavity, γ is the population inversion decay rate, f_r denotes the frequency of relaxation oscillation, η is the normalized pumping rate, Ω_i ($i=p$ or s) is the shift frequency of p - or s -polarized beam, respectively.

Simulated by MATLAB, we found that the closer to the frequency of relaxation oscillation f_r in our system the shift frequency Ω_p and Ω_s are, the larger the frequency-dependent gain factors $G(\Omega_p)$ and $G(\Omega_s)$ are (blue line in **Figure 1c**). However, when the shift frequency (Ω_p or Ω_s) and frequency of relaxation oscillation f_r were too close, it would cause a state of chaos in the spectrum due to the strong nonlinear effect, which is not conducive to the extraction and demodulation of the two feedback beams. Based on the above considerations, the shift frequency Ω_p and Ω_s were set to be 2 MHz and 3 MHz, respectively, enabling the gain factor $G(\Omega_p)$ and $G(\Omega_s)$ of our system reaching 10^4 . Considering that the working frequency of one single AOM was not able to be as low as a few megahertz to meet the conditions set above; thus, we employed two AOMs to acquire a low shift frequency for one optical beam. Specifically speaking (**Figure 1b**), the light with frequency f_0 occurred the positive first order diffraction by AOM₁, resulting that the frequency changed to $f_0 + \omega_1$ ($\omega_1 = 70$ MHz was AOM₁'s working

frequency). After split by PBS, the frequency $f_0+\omega_1$ of the p -polarized light converted to $f_0+\omega_1-\omega_2$ by the negative first order diffraction under the modulation of AOM₂ ($\omega_2=71$ MHz was AOM₂'s working frequency). Finally, the p -polarized light returned to the laser cavity by a mirror (M₁) along the original path, accompanying that the frequency changed to $f_0+\omega_1-\omega_2-\omega_2+\omega_1=f_0+\Omega_p=f_0+2\text{MHz}$ by the combined diffractions of AOM₂ and AOM₁. As similar as the p -polarized light, the s -polarized light split by PBS shared the differential frequency shift process by setting the working frequency of AOM₃ (ω_3) to be 71.5 MHz, indicating that the s -polarized light had a frequency of $f_0+\omega_1-\omega_3-\omega_3+\omega_1=f_0+\Omega_s=f_0+3\text{MHz}$. To verify the accuracy of the simulations, we measured the power spectrum of the system and found the Ω_p and Ω_s to be 2 MHz and 3 MHz, respectively, which were absolutely in accordance with simulations (red line in **Figure 1c**).

In the SPR system, a higher sensitivity corresponds to a larger reflectivity change for a certain RI variation, in which the reflectivity change is affected substantially by the incident angle and the gold film thickness of the SPR chip.²⁰ Calculated by the transfer matrix method (**Note S2**), we found that the reflectivity change reached the maximum 0.237 under the optimal incident angle of 64.01° and the gold film thickness of 52 nm (**Figure 1d**). To further verify the accuracy of the simulations, we set the thickness of gold film at 52 nm and measured the reflectivity curves in pure water, phosphate buffered saline solution and Tris-HCl buffer solution at the incident angles varying from 63° to 67° . As expected, the measured reflectivity curves in three types of solutions were in good agreement with the simulated results (**Figure 1e**). Therefore, to achieve the

193 maximum sensitivity, the incident angle and gold film thickness were set to be 64.01°
 194 and 52 nm, respectively.



195

196 **Figure 1 Detection principle.** (a) Experimental setup of the OLFM-compensated and
 197 LHFI-amplified SPR biosensing platform. L: laser; CL: collimating lens; NPBS: non-
 198 polarized beam splitter; AOM_{*i*} (*i*=1, 2, 3): acousto-optic modulator; QWP: quarter-wave
 199 plate; PBS: polarized beam splitter; M_{*i*} (*i*=1, 2): mirror; PD: photodiode; (b) Schematic
 200 three AOMs-based differential frequency shift module diagram; (c) Simulated gain
 201 factor varying with different shift frequency (blue line) and experimentally measured

power spectrum of the system (red line); (d) Simulated reflectivity changes with gold film thickness and incident angle under the condition of RI variation of 0.002; (e) Relationship between reflectivity and incident angle under the condition of gold film thickness of 52 nm. Type 1 referred to water ($n=1.3242$), Type 2 referred to phosphate buffered saline solution ($n=1.3272$), and Type 3 referred to Tris-HCl buffer solution ($n=1.3357$).

Performance Evaluation for RI Sensitivity. To confirm the stability of the LHFI-amplified SPR system with OLFM compensation approach, we monitored the voltage drift of the measurement channel of *p*-polarized light and the compensation channel of *s*-polarized light, separately (**Figure 2a** and **Movie 1**). We found that the baseline fluctuations responding to water in the *p*-polarized and *s*-polarized light path were relatively large in the 3-hour testing, however, the corrected signal ($U=U_p-U_s$) was significantly improved with stability than that of the measurement channel (U_p) and compensation channel (U_s), indicating the reliability of OLFM compensation approach in minimizing the impact of inherent noise of LHFI-amplified SPR system.

To demonstrate the capability of OLFM-compensated and LHFI-amplified SPR in RI sensing, the sodium chloride (NaCl) solutions at different concentrations were prepared and measured. The real-time signal responses showed significant concentration-dependent changes (**Figure 2b**). The average voltage signals at different RIs corresponding to the solutions of various NaCl concentrations (0.01%–0.1%) were extracted and plotted (**Figure 2c**). Resolution and sensitivity are calculated by the following equation:

224

$$S = \frac{\Delta U}{\Delta n}$$

225

$$Res = \frac{U_{\text{noise}}}{S}$$

226

227

228

where S and Res are the sensitivity and the resolution of RI sensing, respectively. n is the RI of NaCl solution. U_{noise} is the noise value defined as three times the standard deviation of the voltage corresponding to the baseline (6.0×10^{-5} V, **Inset of Figure 2b**).

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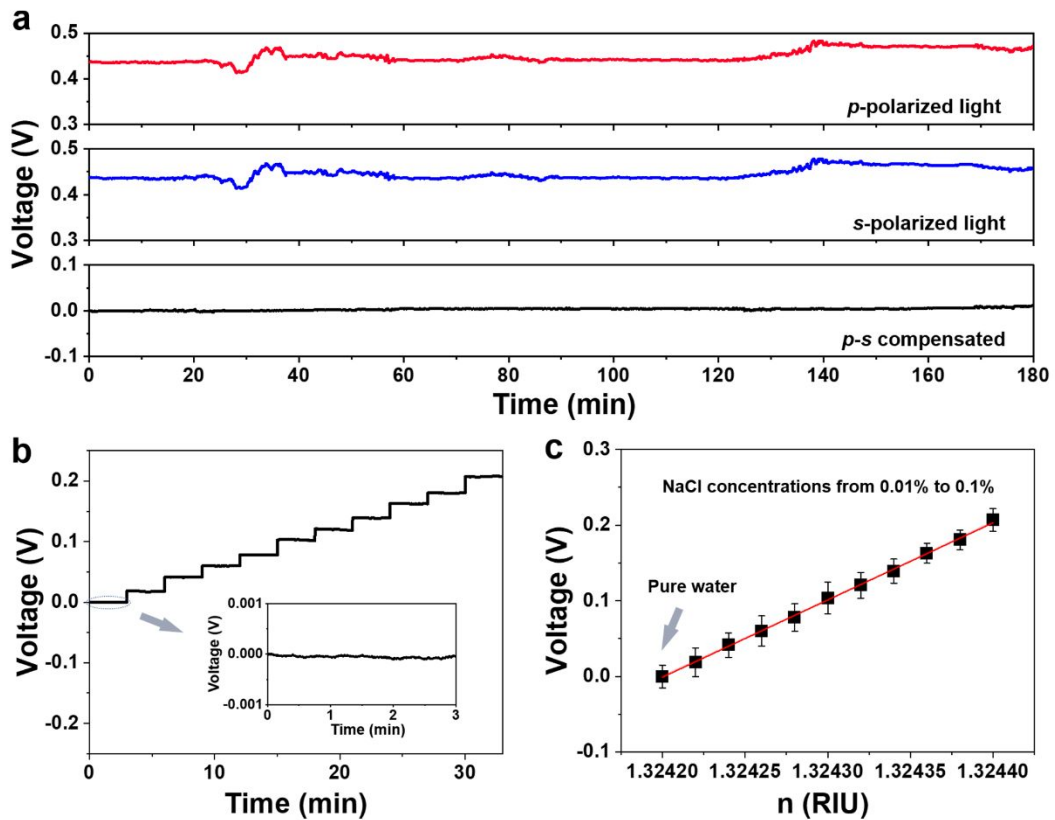
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The resolution and sensitivity of OLFM-compensated and LHFI-amplified SPR system were calculated to be 5.9×10^{-8} RIU and 1.0×10^3 V/RIU, respectively. Compared with the resolution of traditional intensity-modulated SPR system (2.0×10^{-5} RIU, **Figure S2**), that of our SPR system exhibited nearly 3 orders of magnitude enhancement of RI sensing.



234

235 **Figure 2 Performance evaluation of RI sensing.** (a) The 3-hour test results of pure
236 water; (b) Real-time signal responses with different NaCl concentrations ranging from
237 0.01% to 0.1%. Inset: the signal fluctuation corresponding to pure water; (c) The linear
238 fitting curve of the voltage and the RI of NaCl solution.

239 **Biosensing Mechanism with Universality and Versatility.** In order to make the
240 developed SPR device to be a universal biosensing platform capable of detecting a
241 variety of analytical targets, we adopted the most common biological recognition
242 materials and simple biosensing strategies to meet the personalized detection
243 requirement of the target in specific scenarios. As illustrated in **Figure 1a**, nucleic acids,
244 antibodies, and receptors acted as recognition materials to specifically interact with their
245 targets. The presence of analytical targets triggered the surface-based binding between
246 the target and its recognition material via direct binding or indirect competitive
247 strategies, hence changing the RI very close to the gold film of the SPR chip, which had
248 a quantification relationship with the target concentration. The analytical performance
249 of RI-based biosensor is greatly reliant on the approach to anchor functional
250 groups/molecules on the chip surface, i.e., the high-quality surface functionalization to
251 minimum non-specific interferences, providing high target specificity. A well-
252 established gold surface chemistry method was proposed based on the use of thiol-
253 terminated compounds, forming SAMs on gold-coated chip via the Au-S bond (**Note**
254 **S5**). In addition, in order to fully expose functional groups/molecules out of solid surface,
255 spacer arms with different lengths are needed to design and construct by using a series
256 of chemical reactions (**Note S3 and S4**). We adopt a rationally-designed signal readout

method (selected signal after buffer washing, **Note S6**) to avoid the signal disturbance caused by the difference of solution RI between environmental samples.

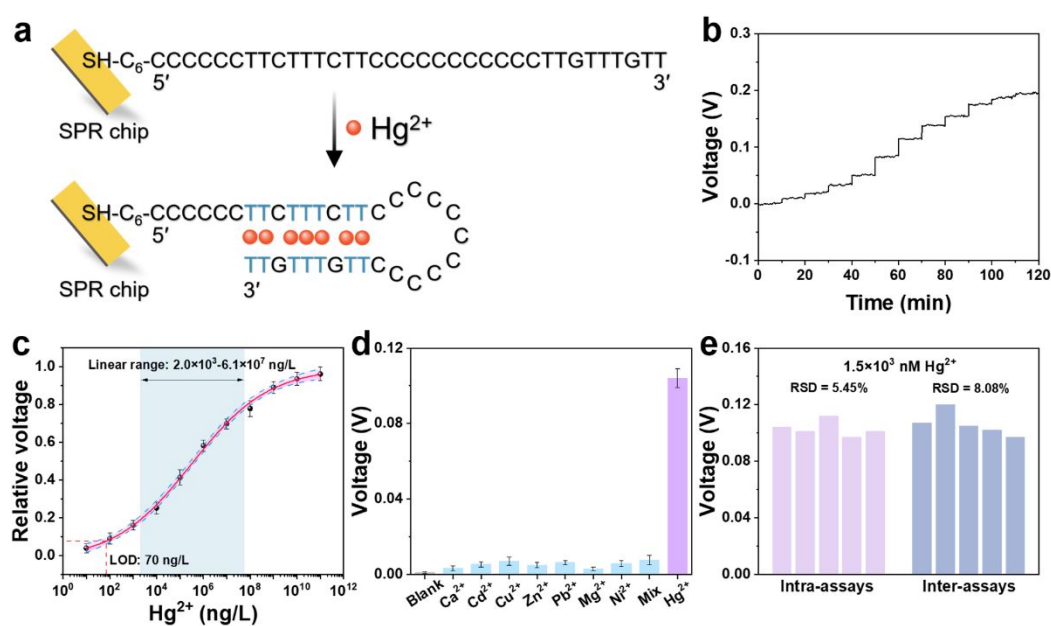
Quantification of Hg²⁺ via Using Nucleic Acid. To test the capability of our SPR system for detection of a broad range of analytical targets by adopting different recognition materials, we first displayed the detection of Hg²⁺ using a Hg²⁺-specific nucleic acid sequence based on the direct binding strategy. Hg²⁺ is a well-known toxic heavy metal, the detection of which is crucial for human health and ecological safety protection. Ono and Togashi first reported that Hg²⁺ ions can specifically and sensitively interact with two thymines for formation of a stable T–Hg²⁺–T structure,²¹ which has been widely exploited to construct various Hg²⁺-specific biosensing techniques. As shown in **Figure 3a**, the Hg²⁺-specific nucleic acid sequence introducing sulfhydryl group on the 5'-end with six methyl groups as the spacer arm (SH-C₆-CCC CCC TTC TTT CTT CCC CCC CCT TGT TTG TT) was immobilized on the SPR chip by the introduction of Au-S bond (**Note S5**). The presence of Hg²⁺ caused the T–T mismatch, promoting the conformation change of the sequence to form the hairpin structure. The Hg²⁺-dependent hairpin structure changed the RI very close to the gold film, which was accurately captured by our SPR system. The real-time SPR signal responses upon the addition of the target Hg²⁺ at different concentrations showed that the signal gradually increased and reached the platform with the increased Hg²⁺ concentration (**Figure 3b**). We fitted the calibration curve of signal response versus target concentration by using a four-parameter logistic model (**Figure 3c**). The relative standard deviations (RSDs) of triple measurement in parallel ranged from 4.7% to 9.6%,

279 showing satisfactory stability. The linear region, defined as 20%–80% inhibition, was
280 observed in the range of 2.0×10^3 to 6.1×10^7 ng/L. According to the rule of 90%
281 inhibition, the limit of detection (LOD) for Hg^{2+} approached 70 ng/L with an RSD of
282 6.9% (n=3). To further demonstrate the analytical performance of our device, we
283 compared it with most previously reported Hg^{2+} biosensor based on the similar T–T
284 mismatch strategy (**Table S1**). Our SPR system outperforms other biosensors in terms
285 of LOD and linear range, confirming the enhanced sensitivity of intensity-modulated
286 SPR sensing by using common-path laser heterodyne feedback.

287 To assess the selectivity of this method, the interference effects of seven metal ions
288 commonly coexisted in matrix, including Ca^{2+} , Cd^{2+} , Cu^{2+} , Zn^{2+} , Pb^{2+} , Mg^{2+} , Ni^{2+} and
289 their mixture on the signal response of this Hg^{2+} -specific nucleic acid-based biosensor
290 were investigated under the same condition (**Figure 3d**). In these experiments, all metal
291 ions were spiked at a final concentration of 1.5×10^3 nM, i.e., EC_{50} , approximately the
292 inflection of standard curve reflecting approximately 50% of the maximum possible
293 response for the target (**Figure 3c**). Except for Hg^{2+} , we observed that the signals of
294 other eight interfering ions were indistinguishable from the blank group, indicating that
295 the good selectivity of the SPR biosensor. On the contrary, the signals in response to
296 Hg^{2+} at both concentrations of 1.0×10^5 and 1.0×10^6 ng/L were negligible if the SPR chip
297 was not functionalized with Hg^{2+} -specific nucleic acid sequences (**Figure S3**).

298 In addition, the intra-assays (five groups synthesized in the same batch) and inter-assays
299 (synthesized in five batches) of the as-prepared Hg^{2+} -specific nucleic acid
300 functionalized SPR chip were evaluated at the Hg^{2+} concentration of 1.5×10^3 nM. The

301 RSDs were 5.45% and 8.08% for intra- and inter-assays, respectively (**Figure 3e**),
 302 indicating the good reproducibility and batch-to-batch precision of the gold surface
 303 chemistry for nucleic acid functionalization.
 304 We evaluated the analytical performance of biosensor for Hg^{2+} in different matrix,
 305 including tap and bottled water. The average recoveries were in the range of 95% to
 306 112% with the acceptable RSDs within 10% in three concentration levels-spiked
 307 samples (**Table S2**), suggesting that this technique exhibited satisfactory accuracy for
 308 Hg^{2+} detection in water matrix.



309
 310 **Figure 3 Performance evaluation of Hg^{2+} -specific nucleic acid-based biosensor.** (a)
 311 Schematic diagram of sensing mechanism for Hg^{2+} ; (b) Signal responses in real-time
 312 with various Hg^{2+} concentrations from 10^1 to 10^{11} ng/L (adding the Hg^{2+} from low to
 313 high concentrations); (c) Standard curve for Hg^{2+} detection fitted with a four-parameter
 314 logistic model. Relative voltage means the ratio of the voltage of different Hg^{2+}
 315 concentrations to the fitted maximum voltage in the four-parameter logistic model; (d)

316 Selectivity of Hg^{2+} detection against other interfering metal ions at the same
317 concentrations of 1.5×10^3 nM. The blank group was the biosensor signal responding to
318 phosphate buffered saline solution; (e) Batch-to-batch intra-assays precision and inter-
319 assays reproducibility of this biosensor.

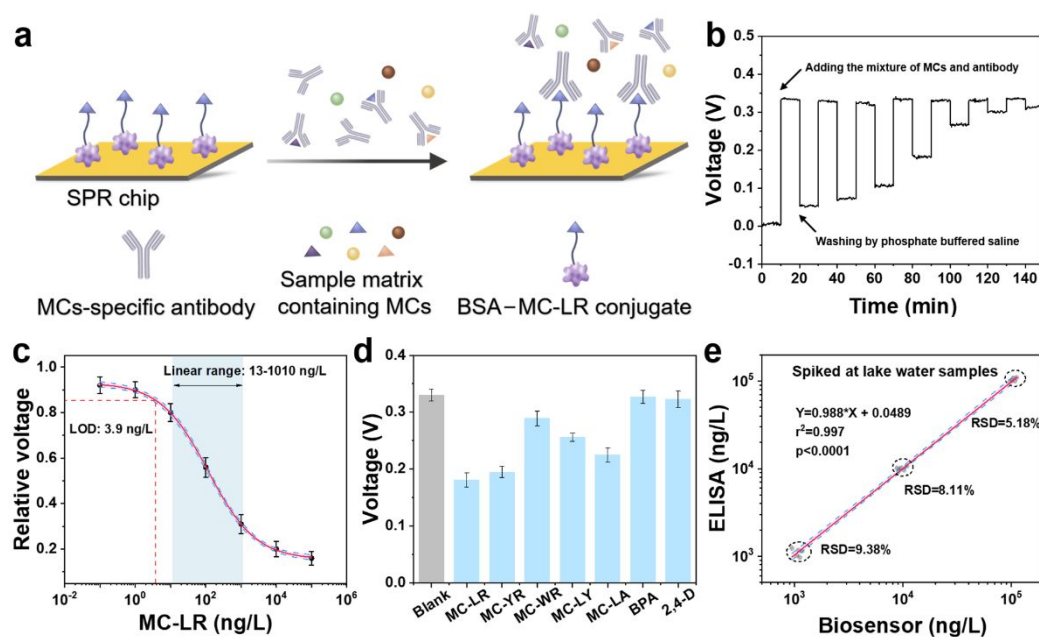
320 **Broad-spectrum Immunoassay for Microcystins.** We further tested the capability of
321 our SPR system to variant-independently detect MCs based on a self-produced group-
322 specific monoclonal antibody presenting both broad-spectrum recognition capabilities
323 and high affinities against MCs.²² MCs are a group of cyclic heptapeptide cyanotoxins
324 with more than 150 variants, being of high toxicity and broad distribution due to the
325 intensified algal blooming events in lakes, and their common routes of exposure include
326 ingestion of contaminated drinking water, food, and algal feed supplements.
327 Considering that the low-molecular-weight MCs targets are hard with different epitopes
328 for the commonly used sandwich immunoassay, we adopted the indirect competitive
329 mode for MCs detection (**Figure 4a**), in which we prepared the BSA–microcystin-LR
330 (BSA–MC-LR) conjugates (**Note S3**) and formed SAMs on the SPR surface via the Au-
331 S bond by introducing a bifunctional crosslinker 11-MUA (**Note S5**). The samples
332 containing MCs were preincubated with the MCs-specific antibody solution to generate
333 the antibody–antigen interaction, and then fed into the sensing unit, so that the unreacted
334 antibody interacted with the immobilized MC-LR on the chip surface, resulting in the
335 changes of RI at the interface. The higher concentrations of MCs in samples would
336 induce the smaller RI change, hence exhibiting a typical “turn-off” sensing mode.

337 The antibody concentration is a critical factor affecting the analytical performance of

indirect competitive immunoassay. We tested the effect of various concentrations of antibody in the range of 0.01 to 10 $\mu\text{g/mL}$ on the signal response and found that the signals increased with the increased antibody concentrations (**Figure S4**). The signals at different antibody concentrations fitted by the four-parameter logistic model demonstrated that the antibody concentrations ranging from 1 to 10 $\mu\text{g/mL}$ represented a sensitive linear region with proportional signal change. To save testing cost, 1.0 $\mu\text{g/mL}$ antibody was selected as the optimal one for use. As a proof-of-concept, the real-time gradient signal responses towards MC-LR, one variant of MCs, at various concentrations ranging from 10^{-1} to 10^5 ng/L were recorded (**Figure 4b**), and the corresponding standard curve was fitted by the logistic model (**Figure 4c**), achieving a LOD of 3.9 ng/L with a linear region from 13 to 1010 ng/L. The ultralow limit detection is nearly 3 orders of magnitude lower than the defined maximal total MCs in drinking water, i.e., 1000 ng/L set by the World Health Organization (WHO).²³ In addition, our biosensor was nearly 2 orders of magnitude sensitive than some commercialized detection techniques such as ENZO MCs enzyme-linked immunosorbent assay (ELISA) kit (LOD up to 100 ng/L)²⁴ with simple and time-saving operating procedures.

To assess the broad-spectrum specificity of this biosensor towards MCs, we tested the signal responses of five MC variants, including MC-LR, microcystin-YR (MC-YR), microcystin-LY (MC-LY), microcystin-WR (MC-WR), and microcystin-LA (MC-LA) at 0.1 nM, i.e., EC_{50} in **Figure 4c**, to see the slightest signal difference in the most sensitive range. Besides, considering that the Adda residue of MCs containing benzene ring is the likely antigenic epitope, hence contributing greatly to the orientation in the

360 binding interaction with the group-specific antibody,²² we also tested the selectivity of
361 this biosensor toward 2,4-dichlorophenoxyacetic acid (2,4-D) and bisphenol A (BPA),
362 both of that contain benzene rings. As expected, all five MC variants showed lower
363 signal responses than that of the blank group due to the “turn-off” sensing mode (**Figure**
364 **4d**). However, the presence of neither BPA nor 2,4-D produced obvious signal change
365 compared with the blank group, indicating that our biosensor was highly selective for
366 MCs. Besides, the gold surface chemistry for protein functionalization also exhibited
367 good reproducibility and batch-to-batch precision within 6.2% of RSDs (**Figure S5**).
368 We measured the lake water samples spiked with 1.0×10^3 , 1.0×10^4 and 1.0×10^5 ng/L of
369 MC-LR, respectively, by using the biosensor and the ELISA method recommended by
370 the U.S. Environmental Protection Agency. We observed that the average recoveries
371 ranged from 89% to 118% with acceptable RSDs less than 10% (n=5) measured by the
372 biosensor (**Table S3**), and both results showed the positive correlation with a strong
373 linear relationship ($r^2=0.997$) (**Figure 4e**).



374

375 **Figure 4 Performance evaluation of MCs-specific antibody-based biosensor.** (a)
 376 Schematic diagram of sensing mechanism for MCs; (b) Signal responses in real-time
 377 with various MCs concentrations from 10^{-1} to 10^5 ng/L (adding the MCs from high to
 378 low concentrations); (c) Standard curve for MC-LR detection fitted by a four-parameter
 379 logistic model as a proof-of-concept. Relative voltage means the ratio of the voltage
 380 with different MC-LR concentrations to the voltage without the addition of MC-LR; (d)
 381 Signal responses towards MC variants and other compounds at the same concentrations
 382 of 0.1 nM. The signal response to phosphate buffered saline solution was defined as the
 383 blank group; (e) Correlation analysis of the detection results between our biosensor and
 384 the standard ELISA method for the spiked MC-LR in lake waters.

385 **Screening of Estrogenic Binding Activity in WWTP.** Lastly, we evaluated the
 386 capability of our SPR system for screening natural and environmental estrogens by
 387 using a nuclear hormone receptor. Natural estrogens have long been known to be the
 388 major sex steroid hormones regulating the development and function of reproductive

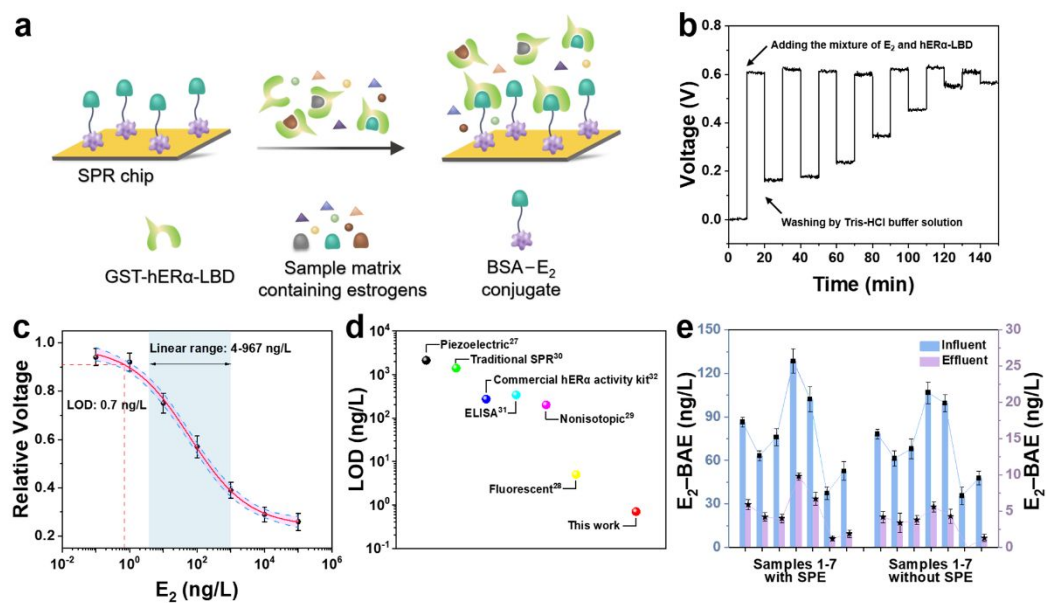
389 organs as well as other functions. Environmental estrogens can mimick the action of the
390 natural estrogens or disturb the signal transduction pathways of estrogens, hence
391 producing the deformity of reproductive system. The affinity interaction between
392 estrogens and nuclear estrogen receptors (nERs) is recognized as one of the molecular
393 initiative events of estrogen signal transduction pathways.^{3, 25} Inspired by this affinity
394 interaction, we designed an indirect competitive-binding assay for screening of
395 estrogenic binding activity (**Figure 5a**). As similar as in **Figure 4a**, we prepared the
396 BSA-17 β -estradiol (BSA-E₂) conjugates (**Note S4**) and functionalized the conjugates
397 on the chip surface (**Note S5**). The sample containing estrogenic binding activity was
398 preincubated with the recombinant human estrogen receptor α ligand binding domain
399 (hER α -LBD), which was described in our previous work.²⁶ The unbound hER α -LBD
400 fed into the sensing unit was then interacted with the immobilized E₂ on the chip surface.
401 And the hER α -LBD induced RI change on the chip surface was accurately captured by
402 the SPR system in a “turn-off” sensing mode.

403 After optimizing the concentrations of hER α -LBD which are critical factors influencing
404 the analytical performance (**Figure S6**), 2.5 μ g/mL hER α -LBD were selected
405 considering both sensitivity and testing cost. We took E₂ as the representative estrogen
406 and recorded the real-time SPR signal responses at various concentrations ranging from
407 10⁻¹ to 10⁵ ng/L (**Figure 5b**), and fitted the standard curve (**Figure 5c**). The LOD for E₂
408 reached 0.7 ng/L with a linear range from 4 to 967 ng/L. We compared the LOD of this
409 method with that of a variety of estrogen receptor-based techniques applied for
410 screening of estrogenic binding activity (**Figure 5d**). Our biosensor outperformed others

411 using different transducers such as piezoelectric,²⁷ fluorescent,²⁸ nonisotopic,²⁹ SPR,³⁰
412 the standard ELISA method,³¹ and commercial estrogenic binding activities kit.³²
413 Compared with many cell-based in vitro assays based on the same binding mechanism
414 between estrogens and nERs, such as ER-CALUX[®],³³ E-Screen assay,³⁴ and the Yeast
415 Estrogen Screen (YES) assay,³⁵ our estrogen receptor-based SPR biosensor not only has
416 obvious sensitivity advantage, but also is cell-free and unaffected by the cytotoxic
417 substances in matrices, especially in environmental samples, hence endowing with
418 satisfactory accuracy and stability.

419 In order to validate the practicability of the developed SPR biosensor, the wastewater
420 samples collected from a WWTP in Tsinghua Campus along treatment processes were
421 tested (**Figure S7**). The wastewater samples, including influent samples and effluent
422 samples, was divided into two groups. One group was directly measured by the
423 developed biosensor after simple filtration, and the other group was enriched by solid-
424 phase extraction (SPE) method and then were diluted to the initial concentration with
425 binding buffer before detection. The estrogenic binding activity of wastewater samples
426 was characterized using E₂-binding activity equivalent (E₂-BAE). As shown in **Figure**
427 **5e**, the influent and effluent samples were 35–128 and 0–9.8 ng/L E₂-BAE, respectively,
428 which was similar to the previously reported results from WWTPs in China, European,
429 and America.³⁶⁻³⁸ The estrogenic binding activities of influent samples were
430 significantly lower than that of effluent samples, which could be attributed to the high
431 removal efficiency of estrogen-active compounds during biodegradation process, such
432 as 89% E₂.³⁹ In addition, the estrogenic binding activities of wastewater samples without

433 SPE were slightly higher than those with SPE, which was easy to understand that there
 434 may be some loss during the extraction and elution process. And the two results
 435 exhibited a good linear relationship (broken lines in **Figure 5e**), illustrating that the
 436 developed SPR biosensor could accurately and reliably detect estrogenic binding
 437 activity in complex wastewater samples without the need for enrichment. We attribute
 438 this great advantage to the ultrasensitivity and the rationally-designed signal readout
 439 method of our SPR system, which can well resist the interference of matrix effect.
 440 Therefore, the SPR biosensor has satisfactory performance for screening of estrogenic
 441 binding activities in real samples.



442
 443 **Figure 5 Performance evaluation of estrogen-specific receptor-based biosensor.** (a)
 444 Schematic diagram of sensing mechanism for estrogens; (b) Signal responses in real-
 445 time with various concentrations of E₂ from 10⁻¹ to 10⁵ ng/L (adding the E₂ from high
 446 to low concentrations); (c) Standard curve for estrogenic binding activity detection fitted
 447 by a four-parameter logistic model by taking E₂ as a proof. Relative voltage means the
 448 ratio of the voltage with different E₂ concentrations to the voltage without the addition

of E₂; (d) Comparison of LOD of our SPR biosensor with other estrogen receptor-based biosensors. The numbers represent the corresponding references in the article; (e) Estrogenic binding activities assay of wastewater samples from the WWTP with and without SPE detected by the biosensor. 1–7 represent samples for 7 days within a week. The E₂-BAE of the influent samples corresponding to the blue scale (left) and that of the effluent samples corresponding to the red scale (right).

ENVIRONMENTAL IMPLICATIONS

This work proposed a polarized light-compensated SPR system with laser heterodyne feedback, resulting in nearly 3 orders of magnitude enhancement of sensitivity over the original SPR system. It utilizes the laser source acting as the emitter, responder, and intrinsic amplifier simultaneously, rarely need optical alignment, and reduces the optical components required, providing a solid research foundation for the development of portable and efficient optical detection devices. In addition, a common-path compensation approach combines the orthogonally-polarized light with frequency multiplexing to resist the interference from environmental noise, which is expected to meet the requirements of on-site inspection.

Based on different recognition materials, the SPR system could achieve the ultrasensitive detection of a variety of analytical targets, from a single small molecule, to a group of chemicals with general structure and their isomers, and to a class of effect-targeting endocrine disrupting activity. Compared with our previous evanescent wave fluorescence biosensor,²⁸ the ultrasensitivity and rationally-designed signal readout method of this SPR system can effectively avoid the interference of matrix effect in

471 complex environmental samples, thus greatly reducing or even avoiding the time
472 consumed by sample concentration, extraction, and enrichment to achieve rapid
473 detection. As a stable and reliable SPR biosensor with ultrasensitivity and universality,
474 it holds promise to revolutionize environmental monitoring, medical diagnostics, and
475 food safety, and provides methodological support for safeguarding environmental and
476 public health.

477 **ASSOCIATED CONTENT**

478 **Supporting Information**

479 The Supporting Information is available free of charge at
480 <https://pubs.acs.org/doi/10.1021/acs.est.xxxxxxx>.

481 Detailed information on materials and reagents, transfer matrix method, synthesis
482 procedures of BSA–MC-LR and BSA–E₂ conjugates, gold surface chemistry,
483 quantification procedures, and sample collection and pretreatment are provided in the

484 **Supporting Information.**

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505 **Notes**

506 The authors declare to no competing financial interest.

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