

RIN and Transmission Performance Improvement Using Second Order and Broadband First Order Forward Raman Pumping

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Abstract— Low RIN bidirectionally pumped Raman amplification is studied. We investigate the importance of the 1st order forward pump generation technique and optimize the forward pump characteristics to achieve RIN comparable with backward only pumping and increased transmission reach.

Keywords—Relative intensity noise; coherent communication; Raman amplification

I. INTRODUCTION

In optical fibre communications systems distributed Raman amplification is used to improve the signal to noise ratio compared with discrete amplification. Bidirectional dual order pumping further improves the optical to signal ratio (OSNR) by reducing the signal power variation along the span compared with conventional first order bidirectional and backward pumping [1,2]. However the improvement in OSNR is counteracted by the impact of relative intensity noise (RIN) transfer from forward pump(s) to signal. Recently many methods have been applied to reduce this RIN transfer such as reducing the front end reflections [3,4], using incoherent pumping [5].

In this paper we use a technique which has some similarity with [5] in that the spectral properties of the forward pump are optimised to improve RIN and consequently transmission performance. We use bidirectionally pumped Raman amplification which has dual order forward Raman pumping: a 1365nm Raman fibre laser provides the 2nd order pump and the first order pump is broadband centred at 1455nm. This technique allows signal RIN suppression to a level comparable to backward only pumping but we show that the method used to generate the broadband first order pump has a significant

impact on both RIN and transmission performance.

We compare two methods to generate the 1st order forward pump experimentally. With optimisation the transmission performance of a 10×100G DP-QPSK WDM system was improved compared with backward only pumping but performance was degraded if the wrong pump generation technique was used. We achieve a signal RIN level of ~ -140dB/Hz with bidirectional pumping and a transmission distance of ~7500km which is an increase of ~400km compared with conventional backward pumping.

II. DISTRIBUTED RAMAN AMPLIFIER SPAN SETUP

Fig. 1 shows the configuration used for the Raman amplifier. In the transmission fibre span (Fig. 1(a)), backward dual order pumping is formed by a 2nd order pump (1365nm) and a high reflectivity (~95%) fibre Bragg grating (FBG) centred at 1455nm. The inclusion of the narrowband (~1nm) FBG gives random lasing at 1455nm near the output end of the span [2,3]. Forward pumping consisted of a 2nd order 1365nm pump and a broadband 1st order pump with 3dB bandwidth ~ 18nm and centred at 1455nm. Only a low 1st order power is required to provide a seed for the Raman amplification and this first order pump seed was generated by backward pumping 10km of G652 standard single mode fibre (SSMF) at 1365nm. The 10km fibre length was used as a compromise between the pump power requirement and 1st order power generation efficiency. The two different methods used to generate this are shown in Fig. 1 (b) and (c).

Scheme-1 shown in Fig. 1 (b) used an open-cavity random fibre laser based configuration without any reflections from either end of the seed generation fibre whereas scheme-2 in

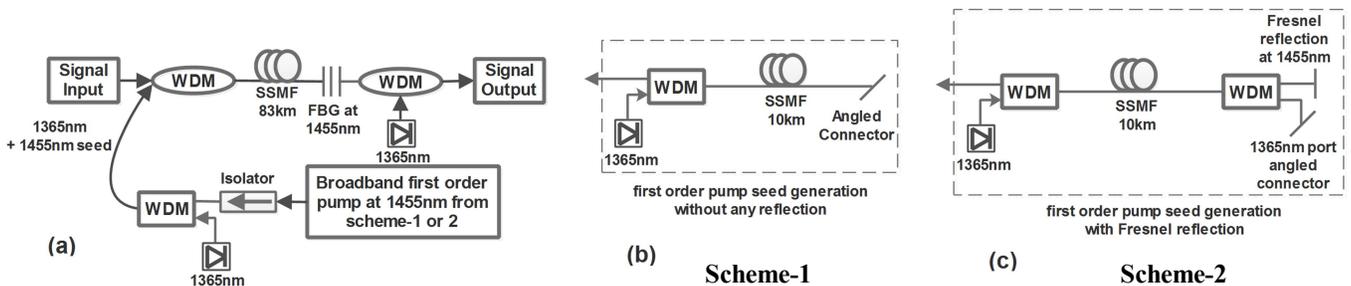


Fig. 1: (a) Schematic of broadband 1st order forward pump based dual order bidirectional Raman span (b) scheme-1: 1st order pump seed generation without any cavity reflections (c) scheme-2: 1st order pump seed generation with 3.4% Fresnel back reflections

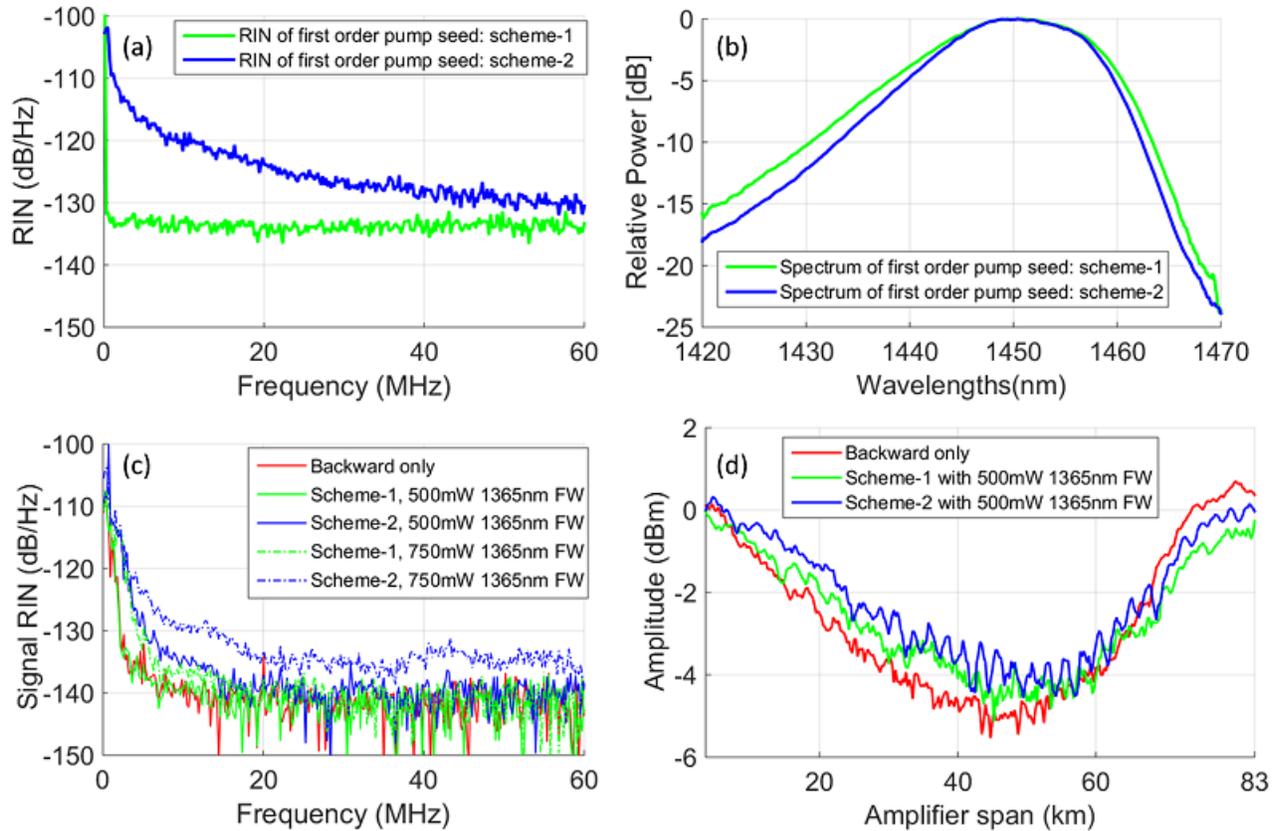


Fig. 2: (a) RIN of 1st order broadband pump seed from two different schemes (b) spectra of 1st order broadband pump seed generated from scheme-1 and 2 (c) signal RIN at 194THz using different Raman pumping schemes (d) signal power profile at 194THz using different Raman pumping schemes

Fig. 1(c) used a very low (~3.4%), broadband (1420~1480nm) Fresnel reflection from the far end of the fibre.

Scheme-1 generated 3mW of first order pump power using 4.5W at 1365nm. In scheme-2 the 1365nm pump power that could be used was limited to 3.5W: higher pump power gave lasing at the Stokes wavelength due to feedback from double Rayleigh backscattering (DRB) [7]. Scheme-2 gave a 1mW 1st order seed at this maximum 1365nm pump power.

The 1st order broadband seed was combined with the 1365nm pump through an isolator. The isolator blocked 1455nm scattered light from the transmission span from entering the seed generation set-up.

III. RIN CHARACTERISATION

The signal RIN performance mainly depends on the RIN transfer from the forward 1st and 2nd order pumps in dual order bidirectional amplifiers.

Fig. 2(a) shows the comparison of the RIN of the 1st order pump generated using scheme-1 and 2. It can be seen that for scheme-1 the RIN level is very low and remains constant at ~ -135dB/Hz, whereas in scheme-2 the RIN is higher, more than -120dB/Hz in the low frequency range. Spectra of the forward 1st order seeds shown in Fig. 2(b) have a similar 3dB bandwidth of ~18nm.

To Raman pump the transmission fibre span forward 1365nm pumping was used with two different powers, 500mW and 750mW. The backward 1365nm pump power was varied between 1 and 1.2W to maintain a 16.5dB on-off gain compensating the loss of the 83.32km standard fibre span.

Fig. 2(c) shows the signal RIN performance and a comparison with backward pumping only. Scheme-1 shows the best performance and is comparable with backward only pumping. The slight increase in signal RIN level in scheme-1 with 750mW of 1365nm pump was mainly due to the transfer from the higher order pump but still remains lower than that of scheme-2 with 500mW. Fig. 2(d) shows the improved signal power profiles of both the schemes compared with backward pumping only.

IV. TRANSMISSION RESULTS AND DISCUSSION

The long haul coherent transmission performance was compared. The lowest signal RIN configurations in both the schemes with 500mW forward 1365nm pump power were used for performance comparison with the backward pumping only case. A re-circulating loop setup with 10×100G DP-QPSK WDM transmission setup was used as shown in Fig. 3. The transmitter consisted of 10 WDM channels (100GHz spaced from 194.3~193.4THz) combined with a 100kHz laser as “channel under test”, a polarisation maintaining EDFA to amplify 30GBaud DP-QPSK modulated WDM signals and a

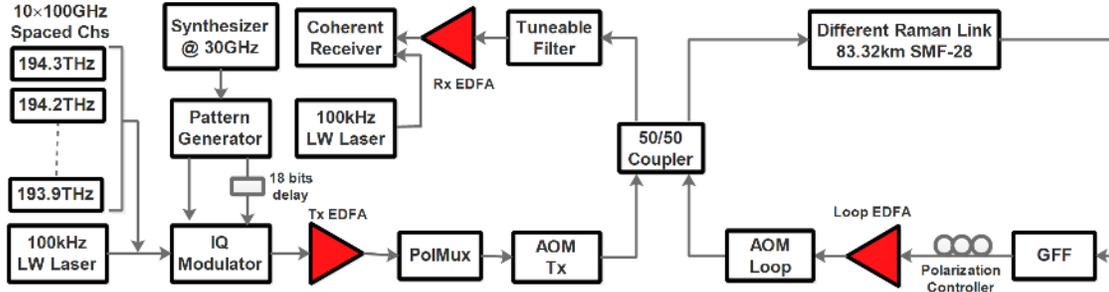


Fig. 3: Experimental setup for long-haul coherent transmission

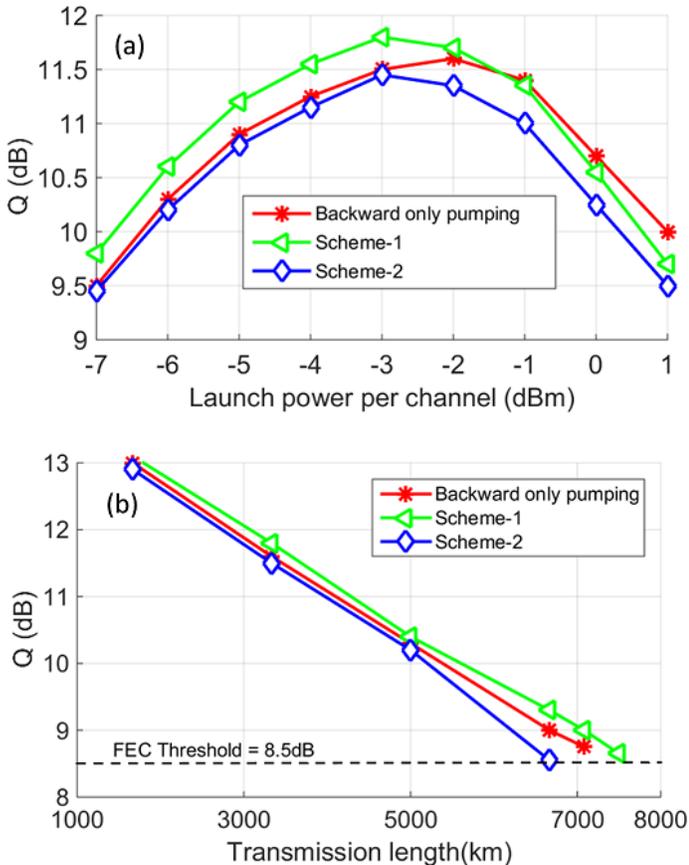


Fig. 4: (a) Q factors versus launch power per channel sweep for the middle WDM channel at 194THz (b) Q factors versus transmission distances at 194THz

polarisation multiplexer. The total loss of the 83.32km Raman span was ~ 17.6 dB including 16.5 dB of fibre loss and ~ 1.1 dB from pump/signal combiner pairs. The additional insertion loss of ~ 12 dB from gain flattening filter (GFF), 50/50 coupler and acousto-optic modulator (AOM) was compensated by using a dual-stage EDFA at the end of the loop. Finally, the output signal was de-multiplexed and amplified by a tuneable filter and an EDFA respectively at the receiver. A polarisation diverse coherent receiver with 80GSa/s, 36GHz bandwidth oscilloscope was used to detect the signal and then offline digital signal processing (DSP) was applied for post

processing. Actual bit error counting over two million bits was used for Q factors calculation.

Fig. 4(a) shows the Q factors versus signal (194THz) launch power per channel at 3333km for different Raman pumping schemes. Q factors improvement of 0.2 dB and 0.4 dB compared with backward pumping only and scheme-2 respectively were observed with scheme-1 at optimum launch power of -3 dBm per channel. This additional improvement comes from comparable signal RIN performance as backward pumping only and improved noise performance by using forward pumping. Although scheme-2 has similar signal power profile to scheme-1 (Fig. 2(d)) and the same 1365nm forward pump power, the worst performance with 0.2 dB degradation of Q factor compared with backward pumping only was mainly due to the high signal RIN transferred from high RIN of the 1st order pump seed. The 1 dB decrease in optimum launch power in both the schemes compared to backward only pumping was expected and caused by higher average signal power along the span leading to additional nonlinearity degradation. Fig. 4(b) shows the Q factors versus transmission distance with different Raman configurations at optimum launch power as shown in Fig. 4(a). Scheme-1 shows the maximum transmission distance of 7499 km with an additional ~ 400 km and ~ 800 km reach enhancement relative to backward only pumping and scheme-2 respectively, due to improved RIN and OSNR performance.

V. CONCLUSIONS

We have demonstrated that RIN transfer in a bidirectionally pumped distributed Raman amplifier can be reduced by using a broadband 1st order Raman pump. We show that the generation process for this broadband pump has an impact on RIN and consequently transmission performance. With optimisation the performance of the forward pumped system had RIN comparable with backward only pumping but improved transmission performance. However with an inappropriate broadband pump generation scheme both RIN and transmission performance were degraded.

In conclusion, for a 10x100G DP-QPSK WDM system, broadband 1st order pump generation using an open-cavity random lasing configuration allowed a ~ 400 km transmission reach increase to ~ 7500 km compared with conventional backward pumping only.

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